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RDTE PROJECT NO.  
USAAVSCOM PROJECT NO. 69-01  
USAASTA PROJECT NO. 69-01

**AIRWORTHINESS AND FLIGHT CHARACTERISTICS  
AH-1G HELICOPTER WITH  
STABILIZED NIGHT SIGHT (SNS)**

**PHASE I**

**FINAL REPORT**

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PROJECT ENGINEER

MARVIN W. BUSS  
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**DECEMBER 1969**

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US ARMY AVIATION SYSTEMS TEST ACTIVITY  
EDWARDS AIR FORCE BASE, CALIFORNIA 93523

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USAAVSCOM PROJECT NO. 69-01  
USAASTA PROJECT NO. 69-01

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## ABSTRACT

The Phase I airworthiness and flight characteristics tests of the AH-1G helicopter with the mock-up stabilized night sight (SNS) installed indicated a feasibility for further development utilizing the actual SNS equipment. No significant changes in the handling qualities due to the SNS modification were noted during the tests. The static, proof load test results indicate that the structure is adequate to withstand the required loads. The flight test data from the three nonrotating control boost tubes show higher loads for the AH-1G in both the SNS and standard nose configurations than the Bell Helicopter Company test data. The control boost tube loads reached the maximum permitted at conditions short of the published envelope. Testing was terminated early to obtain instrumented components (rotor blade, drag brace and pitch link) so the flight envelope and/or fatigue life of these components could be more accurately determined. These tests are scheduled to be completed during Phase II with the actual SNS installed. The vertical six-per-revolution vibrations at the copilot's seat exceed military specification requirements in the SNS configuration.

## TABLE OF CONTENTS

	<u>Page</u>
INTRODUCTION. . . . .	1
Background. . . . .	1
Test Objectives . . . . .	1
Description . . . . .	1
Scope of Test . . . . .	2
Method of Test. . . . .	3
Chronology. . . . .	4
RESULTS AND DISCUSSION. . . . .	5
Static, Proof Load Tests. . . . .	5
Airworthiness and Structural Loads Tests. . . . .	5
Performance . . . . .	8
Stability and Control . . . . .	8
Vibration . . . . .	8
CONCLUSIONS . . . . .	9
RECOMMENDATIONS . . . . .	10
APPENDIXES. . . . .	11
I. References. . . . .	11
II. Test Data . . . . .	12
III. Test Instrumentation. . . . .	37
IV. Standard AH-1G Operating Limitations and Dimensions . . . . .	39
V. Distribution. . . . .	41

# INTRODUCTION

## BACKGROUND

1. The stabilized night sight (SNS) system is being developed to improve the night tactical operations capability of various weapons systems currently in the Army inventory. The SNS is being developed by the Itek Corporation for the US Army Mobility Equipment Research and Development Center under contract number DAAK-02-78-C-0491. The design and initial testing of the SNS is being accomplished by Itek Optical Systems Division (OSD), Burlington, Massachusetts. The fabrication of attachment structure and the installation of the mock-up SNS and functioning system are being accomplished by Itek Lincoln Aerospace Division (LAD), Lincoln, Nebraska. Since installation of the SNS on the AH-1G required significant modification of the basic aircraft structure and external shape, the US Army Aviation Systems Command (USAAVSCOM) was designated to evaluate the airworthiness and flight characteristics (A&FC) tests on the AH-1G, S/N 66-15293, in two phases. The first phase determined the feasibility of installing the system on the AH-1G by conducting tests with a mock-up SNS installed. The second phase will evaluate the aircraft with the actual SNS installed and also provide the data to issue a safety-of-flight release for further SNS performance and operational capability tests. The static test methods, results and conclusions are described in reference 1, appendix I.

## TEST OBJECTIVES

2. The objectives of the Phase I test program were as follows:
  - a. Determine the structural adequacy of the SNS installation on the AH-1G by static, proof load testing.
  - b. Determine A&FC of the AH-1G with a mock-up SNS installed.
  - c. Obtain quantitative and qualitative data to develop a flight envelope and safety-of-flight release for further prototype functional and operational testing with a functional SNS installed.

## DESCRIPTION

3. The tests were conducted on a standard AH-1G helicopter, S/N 66-15293, with the XM28 weapon system installed prior to structural

modification forward of fuselage station (FS) 61 in order to install the mock-up SNS. The aircraft was instrumented to record stability and control parameters; limited performance parameters; structural load data in the mock-up SNS and attachment areas; span, chord and torsion loads on the horizontal stabilizer and nonrotating control boost tube axial loads. The data were recorded for each test condition on a 50-channel oscillograph mounted in the ammunition compartment.

4. The SNS is a multipurpose viewer having a modular design capability as follows:

a. Provides the user a sight for accurate aiming of aircraft mounted weapons at night.

b. Provides high resolution surveillance and target acquisition from moving vehicles.

c. Provides remote viewing for operational control by using a flexible fiber optic rope.

5. The mock-up SNS was installed in the nose of the AH-1G forward of FS 46. The mock-up was designed to have the same external shape and the same mass distribution as the production SNS. The weight of the mock-up was 285 pounds. One hundred pounds of ballast were installed in the tail above the stinger attachment to maintain the center of gravity (cg) within limits.

#### SCOPE OF TEST

6. Phase I of the A&FC tests was limited in scope to obtaining structural, control load and stability and control data for those test conditions established as the envelope was expanded. Testing was conducted at Edwards Air Force Base, California, and the minimum usable density altitude ( $H_D$ ) was 5000 feet.

7. Eighteen flights were conducted totaling 11.5 hours.

8. The test conditions are shown in table 1.



Table 1. Test Conditions.

Aircraft Configuration <sup>1</sup>	Gross Weight (lb)	Average Density Altitude (ft)	Mid Center of Gravity (in.)	Rotor Speed (rpm)	Mock-up SNS
Clean	7560	5000	195.8	324	Installed
Clean	7560	5000	195.8	324	Removed
Clean	8610	5000	197.1	324	Installed
Hog	8415	5000	194.5	324	Installed
Hog	9270	5000	194.5	324	Removed
Hog	9270	5000	194.5	324	Installed

<sup>1</sup>The clean configuration had no wing stores; the hog configuration had two XM159 pods on each wing.

#### METHOD OF TEST

9. The method used during envelope expansion was to increase the airspeed, normal acceleration and maneuver rates in increments. The data from each flight were processed and analyzed before determining the test conditions for the next flight. Standard configuration loads and control characteristics data used for comparison were obtained from previous USAASTA and Bell Helicopter Company (BHC) flight test reports (ref 2, app I). Limited base-line data were obtained with the test aircraft in a standard nose configuration. Static stability characteristics were determined from data recorded during stabilized flight in each of the desired conditions within the developed flight envelope. Dynamic stability and controllability were qualitatively evaluated and compared with the standard AH-1G characteristics throughout the conduct of the test.

#### CHRONOLOGY

10. The chronology of the Phase I test program is as follows:

Test helicopter received	5 March	1969
Test directive received	18 March	1969
Test plan submitted	April	1969
Static, proof load tests completed	10 May	1969
Flight testing initiated	29 May	1969
Flight testing completed	26 June	1969
Aircraft delivered to contractor for installation of SNS	30 June	1969
Draft report submitted	October	1969

## RESULTS AND DISCUSSION

### STATIC, PROOF LOAD TESTS

11. The results and discussion of the static, proof load tests conducted by USAASTA and National Aeronautics and Space Administration (NASA) personnel at the NASA Flight Research Center's high-temperature loads calibration facility are contained in the Flight Research Center's working paper (ref 1, app I). The concluding remarks of this paper state the following:

a. All the static load tests on the AH-1G helicopter requested by USAASTA, Edwards Air Force Base, California, were performed without damage of any kind to the vehicle.

b. The structural displacements were small, and no evidence of incipient failure was observed.

c. All measured strains and stresses appeared to be well below the yield strengths of the materials upon which the strain gages were mounted.

### AIRWORTHINESS AND STRUCTURAL LOADS TESTS

12. The data for the structural loads in the mock-up SNS and attachment structure for all conditions tested indicated lower stress levels than those experienced during the static, proof load tests. Visual inspection of the critical areas at the completion of the testing revealed no evidence of cracking or fatigue damage.

13. Additional strain gage instrumentation was installed on the three nonrotating control boost tubes for the flight tests. These parameters were selected as indicators of any increase in loads in the critical areas of the rotating components due to the SNS modification. The maximum allowable load value for the three control boost tubes was established by AMSAV-R-FS and was forwarded to USAASTA in letters dated 27 March 1969 and 1 July 1969. The limit value for the flight testing was 2000 pounds (oscillatory) in any one of the control boost tubes. The oscillatory control boost tube data (one-half peak to peak) are presented in figures 1 through 15, appendix II.

14. The data show load values approaching the defined limit of  $\pm 2000$  pounds at conditions well short of the published AH-1G operating envelope. Testing in the SNS configuration was limited to

those conditions where the maximum allowable load was not exceeded since the critical rotating components were not instrumented. To obtain reference data, flights were then flown in the standard nose configuration. The control boost tube load values were less in this configuration but they still exceeded the defined limit of  $\pm 2000$  pounds for some conditions. The maximum ( $\pm 2600$  pounds) longitudinal boost tube load was recorded in the standard nose configuration at: 141.5 knots calibrated airspeed (KCAS), a 2.35g normal acceleration, a 7560-pound gross weight (grwt) and a density altitude of 5000 feet. The following was shown by the data:

a. In the standard nose configuration, oscillatory load data obtained in level flight at a 5000-foot  $H_D$  agree (within 100 pounds) with the interpolated BHC data for both the longitudinal and collective boost tubes. The lateral boost tube data show higher loads (maximum deviation was 200 pounds) for the test aircraft.

b. With the mock-up SNS installed, oscillatory load data obtained in level flight at a 5000-foot  $H_D$  and a 9270-pound grwt show maximum load increases of 100 pounds in the longitudinal boost tube, 300 pounds in the lateral boost tube and 50 pounds in the collective boost tube. At a 7560-pound grwt and a 5000-foot  $H_D$ , the boost tube loads for level flight show very little difference due to the SNS installation.

c. During symmetrical pullouts at 116.5 KCAS with the standard nose installed, the longitudinal and collective boost tube loads recorded are approximately 100 pounds greater than the BHC data at 2.0g's. The lateral boost tube loads are approximately 200 pounds greater than the BHC data at 2.0g's. During symmetrical pullouts at 141.5 KCAS, collective boost tube loads recorded show reasonable agreement with the BHC data. The longitudinal and lateral boost tube loads, however, are approximately 400 pounds greater at 2.0g's than the BHC data. Under these conditions, the longitudinal boost tube loads reach 2000 pounds at an approximate 2g normal acceleration.

d. For dive airspeeds greater than maximum airspeed for level flight ( $V_H$ ), reduced power settings for the same airspeed results in a reduction of the boost tube loads. For constant power settings less than maximum, the rate of increase in the boost tube loads with increasing airspeed is the same as that at the maximum power setting.

e. At airspeeds above 140 KCAS using maximum power at a 7560-pound grwt and a 5000-foot  $H_D$ , the longitudinal boost tube loads increase with airspeed similarly to a linear extrapolation of BHC level-flight data and reach 2000 pounds at 170 KCAS. The lateral

boost tube loads increase moderately with airspeed; whereas, an extrapolation of BHC data indicates a slight decrease. The collective boost tube loads increase rapidly with airspeed from approximately 450 pounds at 140 KCAS to 2000 pounds at 180 KCAS. BHC data at a 6500-pound grwt show a similar trend (only BHC data presented above 140 KCAS at 5000 feet).

f. With the mock-up SNS installed, the loads during symmetrical pullouts were greater for all three control boost tubes. At 116.5 KCAS and a 2g normal acceleration, the recorded loads were approximately 450 pounds greater in the longitudinal boost tube, 550 pounds greater in the lateral boost tube and 400 pounds greater in the collective boost tube than the data for the test aircraft with the standard nose installed. At 141.5 KCAS and a 1.4g normal acceleration, the increase was approximately 150 pounds in the lateral boost tube and 50 pounds in the collective boost tube. The longitudinal boost tube loads data were inconclusive at 141.5 KCAS.

g. The technique used to obtain loads data during this test program was to use the maximum collective setting (power required for  $V_H$ ) for all dive air speeds above the design  $V_H$ . Data were also obtained at 150 KCAS to determine the effect of reduced collective settings and increased dive angles on the boost tube loads at an airspeed greater than  $V_H$ . The results presented in figures 1, 2 and 3 show a significant reduction in the loads as the collective was reduced and the dive angle was increased.

h. The technique used during the symmetrical pullout tests was to maintain the level-flight collective setting throughout the maneuver. The desired normal acceleration (g) was established by making a smooth cyclic input such that the target g and airspeed were obtained as the aircraft passed through the level flight attitude. The target conditions of g and airspeed can also be obtained by establishing constant airspeed and cyclic induced pitch rates and then applying various collective inputs to achieve the desired g values. The qualitative opinion is that the two techniques will produce significantly different loads in the rotor system.

15. The higher boost tube loads data (higher than BHC) indicate a potential problem for the SNS configured AH-1G either in fatigue life of the critical rotating components or in operating envelope. The higher-than-expected control tube loads in both nose configurations should be further studied. Further flight tests with all critical rotating components instrumented should be conducted during Phase II tests to determine the cause of the increased loads and what effect the new load values have on the fatigue life of the components.

### PERFORMANCE

16. Performance data were not obtained during the Phase I tests due to the restricted envelope available and the early curtailment of the flight tests.

### STABILITY AND CONTROL

17. The results of the static longitudinal stability and static lateral-directional stability tests are shown in figures 16 through 20, appendix II. No significant differences from standard AH-1G characteristics were noted. Qualitative evaluations of the controllability and dynamic stability characteristics indicate that no significant differences existed in the handling qualities of the AH-1G with the mock-up SNS installed.

### VIBRATION

18. The results of the vibration tests are shown in figures 21 through 24, appendix II. The vibration data were recorded at the copilot's position for vertical and lateral accelerations. The data indicate no significant differences between standard nose and the mock-up SNS configurations for one- and two-per-revolution frequencies. The vertical six-per-revolution vibration is slightly greater (0.1g) for the SNS configuration at light gross weight and considerably greater at the heavy gross weight in the hog configuration. The vertical six-per-revolution vibrations were 32.4 Hertz with the mock-up SNS installed and exceeded the vibration requirements of paragraph 3.7.1(b), MIL-H-8501A (0.15g below cruise airspeed and 0.2g above cruise airspeed). The lateral four-per-revolution vibrations were 21.1 Hertz and exceeded the specification in the standard configuration at light gross weight above cruise airspeed ( $V_{cruise}$ ).

## CONCLUSIONS

19. The tests indicate no significant change in the handling qualities of the AH-1G helicopter due to the installation of the mock-up SNS (para 17).

20. The cause of the higher loads in the nonrotating control boost tubes and its effect on the fatigue life of critical components must be further analyzed when data from the Phase II tests are available. Since the data indicate higher loads for both the standard and SNS configurations, the fatigue life and flight envelope may be affected for all AH-1G aircraft (para 15).

21. The vibration data show that the vertical six-per-revolution (32.4 Hertz) and lateral four-per-revolution (21.1 Hertz) vibration exceed the limits of MIL-H-8501A (para 18).

22. Further testing with a production SNS installed and in the standard configuration is required to define the flight envelope, performance and fatigue life of the main rotor (paras 15 and 16).

## RECOMMENDATIONS

23. Further testing with a production SNS installed on the AH-1G should be accomplished to provide the required performance and load data so a flight release can be defined (para 22).

24. Future flight loads surveys should be conducted to the limits of any proposed operating envelope, and the techniques for achieving the required test conditions should be clearly defined (para 20).

25. The six-per-revolution vertical vibration with the SNS installed should be reduced to the levels specified in MIL-H-8501A (para 21).



## APPENDIX I. REFERENCES

1. Working Paper, National Aeronautics and Space Administration (NASA) Flight Research Center, *Static Load Tests of a Simulation Package on an AH-1G Helicopter*, 11 July 1969.
2. Report, Bell Helicopter Company, 209-947-041, *Specification for Flight Load Survey on the Model AH-1G Helicopter*, 18 July 1966.
3. Letter, with inclosure, USAAVSCOM, subject: Test Directive, USAAVSCOM, No. 69-01, "Airworthiness Qualification of the Stabilized Night Sight on the AH-1G," 18 March 1969.
4. Test Plan, USAASTA, Project No. 69-01, *Airworthiness and Flight Characteristics of the AH-1G with Stabilized Night Sight (SNS)*, June 1969.
5. Military Specification, MIL-H-8501A, *Helicopter Flying and Ground Handling Qualities; General Requirements For*, with Amendment 1, 3 April 1962.
6. Letter, USAASTA, subject: Interim Progress Report, Airworthiness and Flight Characteristics Tests of the Stabilized Night Sight on the AH-1G Helicopter, 16 June 1969.
7. Letter, USAASTA, subject: Airworthiness and Flight Characteristics Tests of the Stabilized Night Sight on the AH-1G Helicopter, 17 July 1969.
8. Message, USAAVSCOM, AMSAV-P-FS, subject: Safety -of-Flight Release for Flight Test of the Itek Stabilized Night Sight, 24 May 1969, (Unclassified).

## **APPENDIX II. TEST DATA**

**FIGURE 1b. 1**  
**LONGITUDINAL BOOST TUBE LARRE DURING FORWARD FLIGHT**  
**RH-1G USA SN 66-15238**

	DENSITY	GROSS	G.W.	STATIC	STATIC
	ALTITUDE	WEIGHT	WEIGHT	WEIGHT	WEIGHT
SYMBOL	ALT.	W.LB.	W.LB.	W.LB.	W.LB.
○	5000	7560	135.8	389	CLEAN, STD. NOSE
□	5000	7560	135.8	389	CLEAN, SUS(CLOSED)

**NOTE:**

- 1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY REPORT LR 200-093-041 INTERPOLATED TO 5000 FEET AND 7560 POUNDS.
- 2- OPEN SYMBOLS DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT OR MAXIMUM POWER DURING DESCENDING FLIGHT.
- 3- TRIANGLES DENOTE 30 PSI TORQUE.
- 4- FLASCS DENOTE 35 PSI TORQUE.

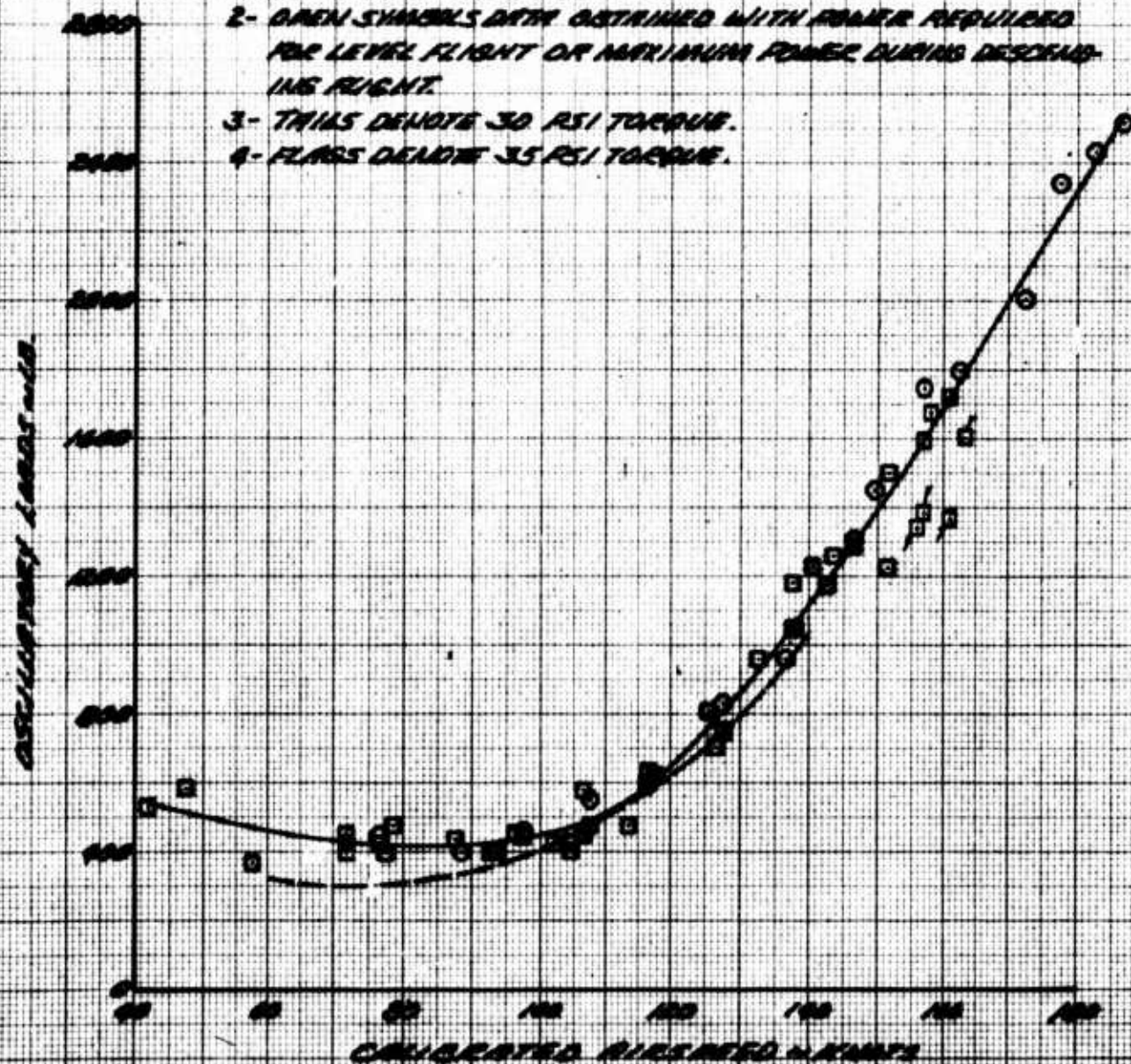
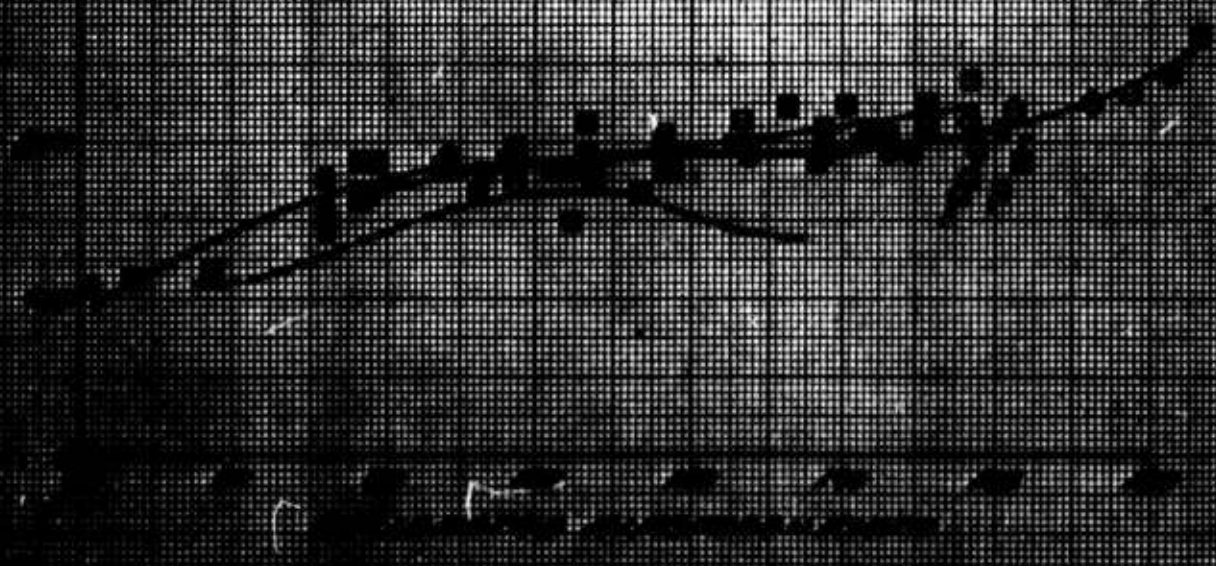




Figure 10-2  
 Comparison of the Two Data Series for the River  
 from 1950 to 1955

	1950	1951	1952	1953	1954	1955
Series 1	100	110	120	130	140	150
Series 2	100	110	120	130	140	150

1. The data series for the river from 1950 to 1955 are shown in the figure.
2. The data series for the river from 1950 to 1955 are shown in the figure.
3. The data series for the river from 1950 to 1955 are shown in the figure.
4. The data series for the river from 1950 to 1955 are shown in the figure.

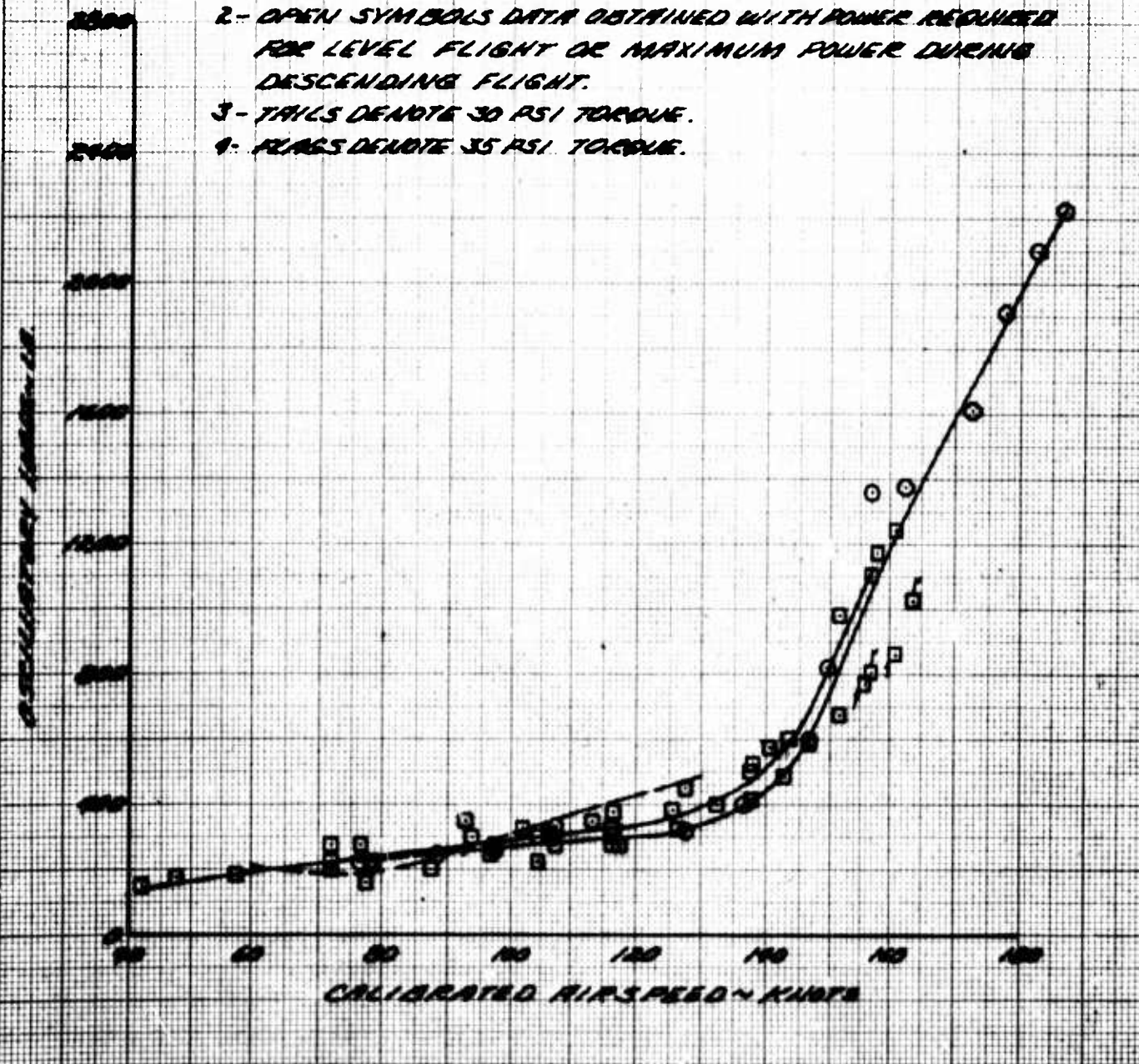


**FIGURE NO. 3**  
**COLLECTIVE BOOST TUBE LOADS DURING FORWARD FLIGHT**  
**AH-1G USA SIN 66-15293**

	DENSITY	GROSS	C.G.	ROTOR	
	ALTITUDE	WEIGHT	STATION	SPEED	
SYMBOL	FT.	LB.	IN.	RPM	CONFIGURATION
○	5000	7560	195.8	329	CLEAN, STD. NOSE
□	5000	7560	195.8	329	CLEAN, SNS (CLOSED)

**NOTE:**

- 1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY REPORT NO. 209-039-081 INTERPOLATED TO 5000 FEET AND 7560 POUNDS.
- 2- OPEN SYMBOLS DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT OR MAXIMUM POWER DURING DESCENDING FLIGHT.
- 3- TAILS DENOTE 30 PSI TORQUE.
- 4- FLAGS DENOTE 35 PSI TORQUE.



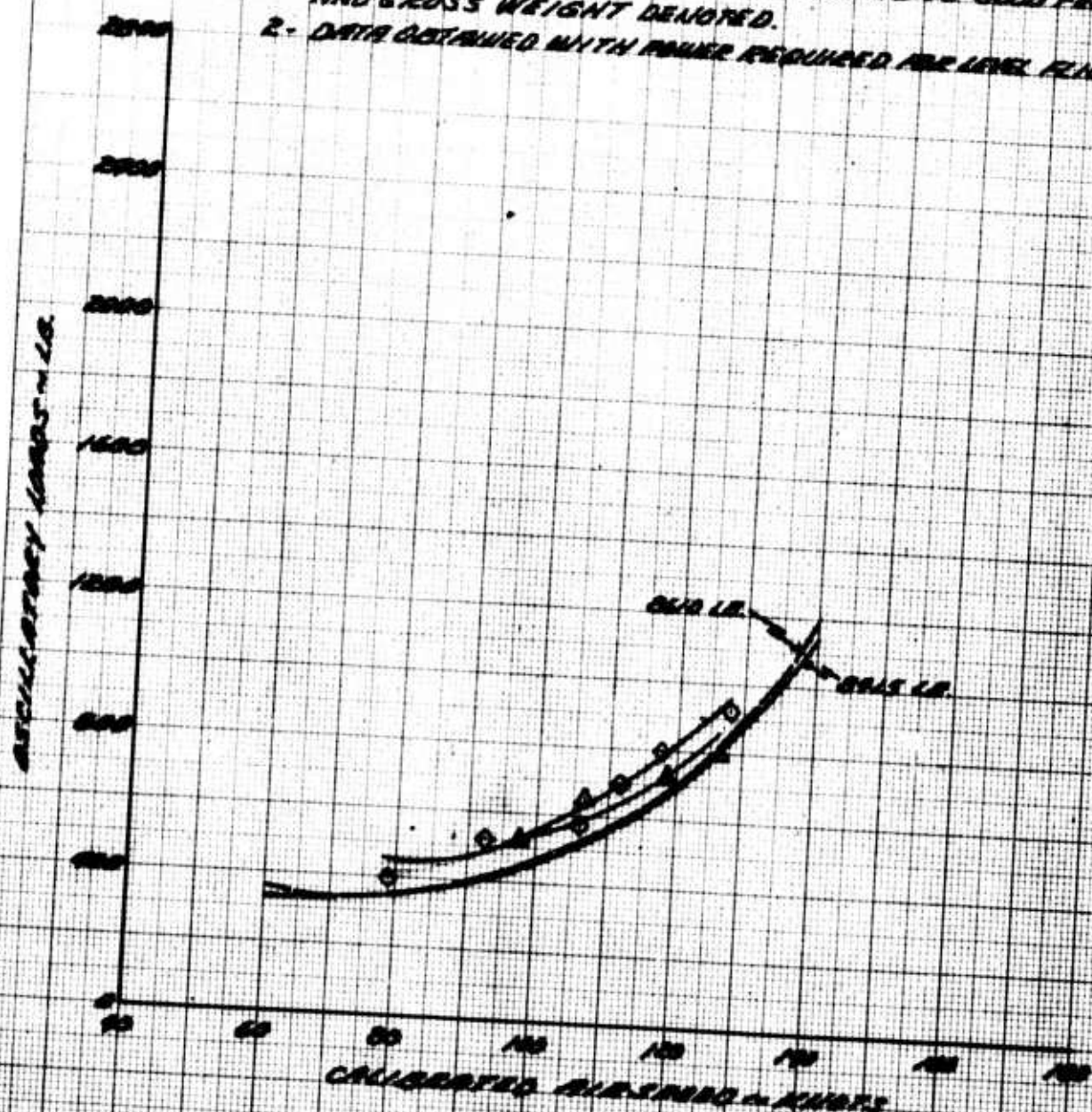


**FIGURE No. 9**  
**LONGITUDINAL Burst Tube Loads During Forward Flight**  
**AH-1G USA SIN 66-15293**

	DENSITY	GROSS	O.B.	ROTAL	
SYMBOL	ALTITUDE	WEIGHT	STATION	SPEED	CONFIGURATION
	in FT.	in LB.	in IN.	in MPH	
●	5000	8615	189.5	300	HOSS, SAS (CLOSED)
Δ	5000	8610	188.1	320	CLEAN, SAS (CLOSED)

**NOTE:**

- 1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY REPORT NO. 203-033-0A1 INTERPOLATED TO 5000 FEET AND GROSS WEIGHT DENOTED.
- 2- DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT.

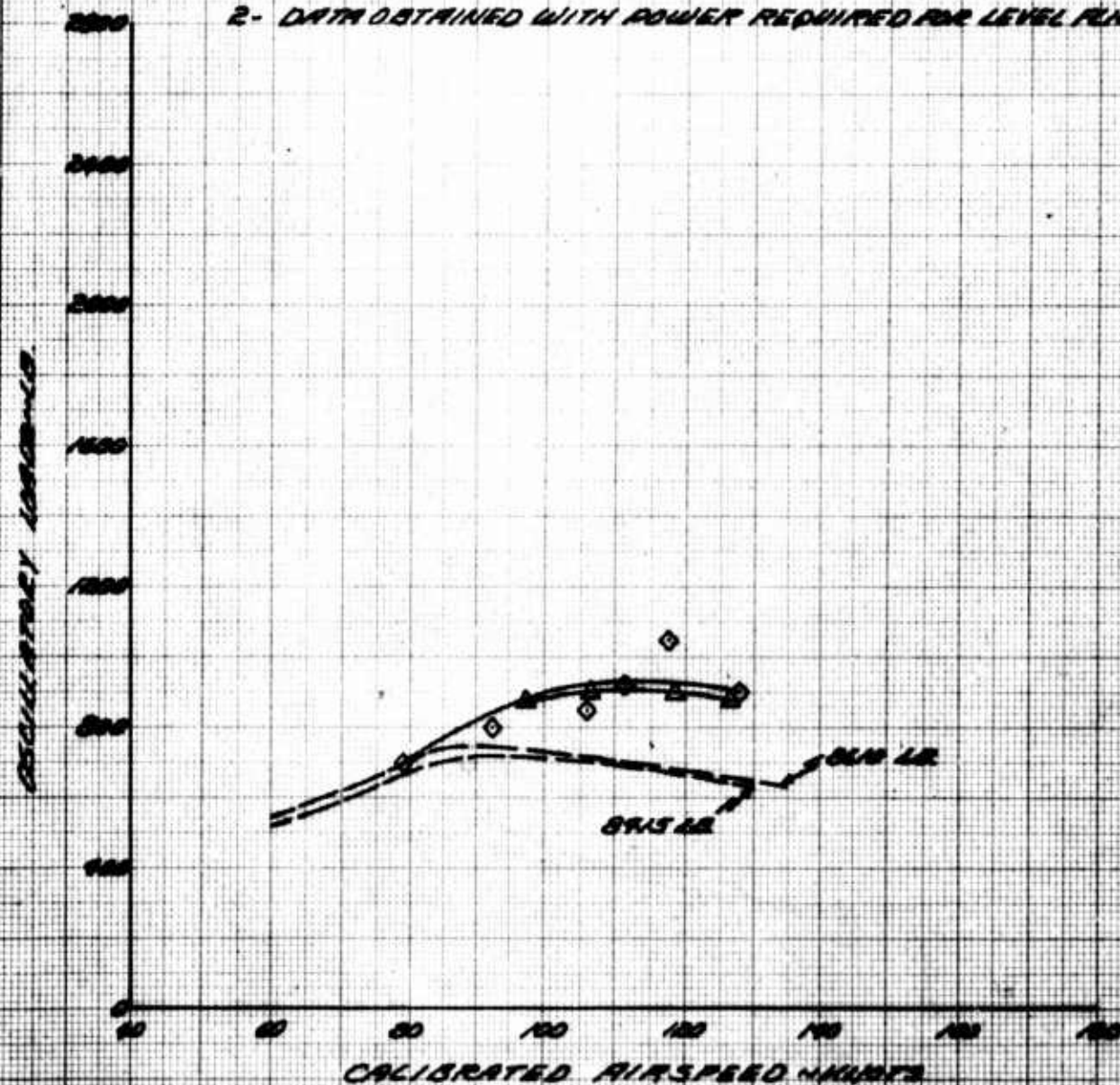


**FIGURE No. 3**  
**LATERAL BOOST TUBE LOADS DURING FORWARD FLIGHT**  
**AH-1G USA SIN 66-15293**

	DENSITY	GROSS	C.G.	ROTOR	
	ALTITUDE	WEIGHT	STATION	SPEED	
SYMBOL	WFT.	N LB.	NIN.	WPM	CONFIGURATION
◇	5000	8915	199.5	324	NOB, SAS (CLOSED)
△	5000	8610	197.1	324	CLEAR, SAS (CLOSED)

**NOTE:**

- 1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY REPORT NO. 209-039-081 INTERPOLATED TO 5000 FEET AND GROSS WEIGHT DENOTED.
- 2- DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT.



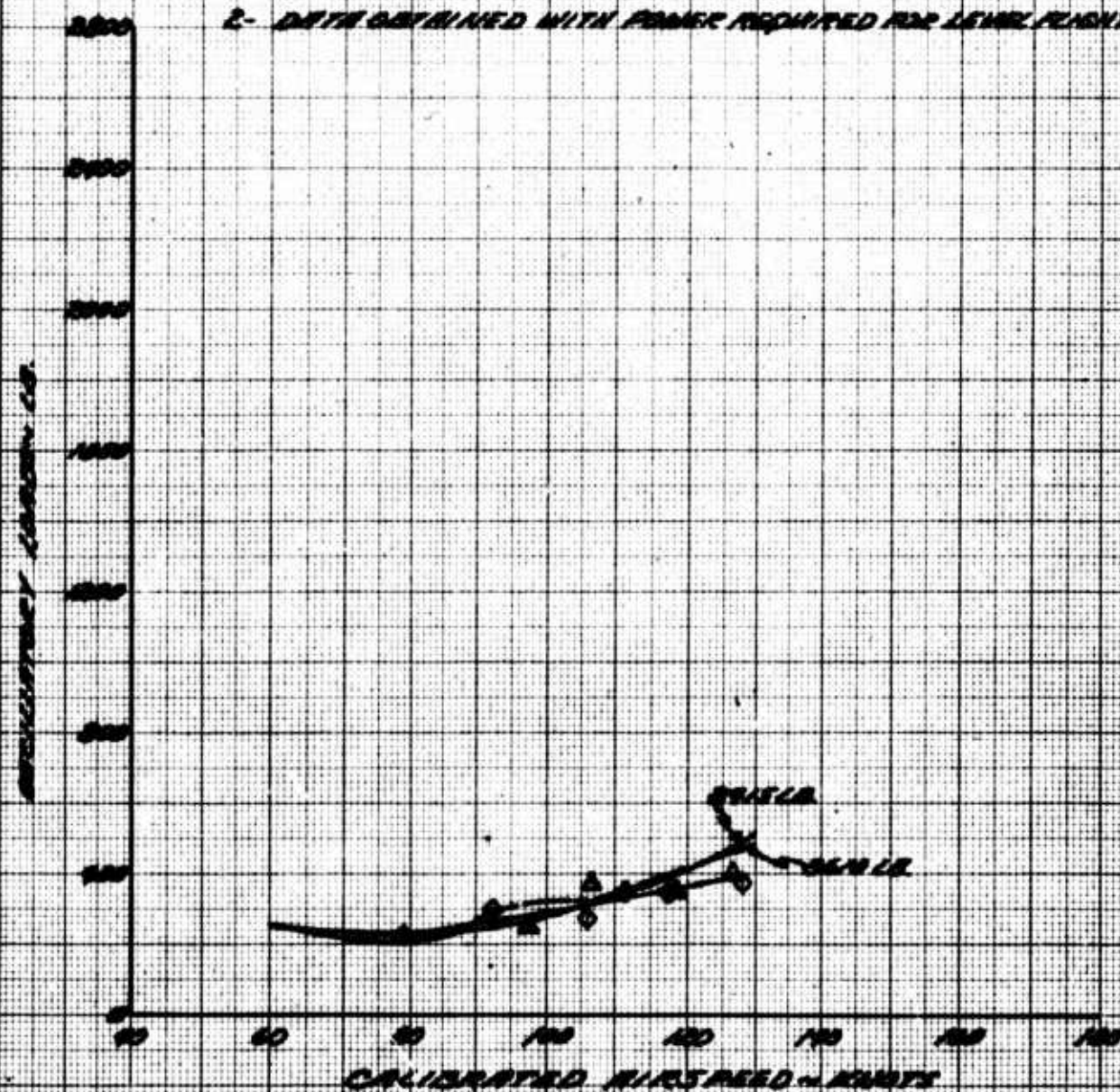


**FIGURE No. 6**  
**COLLECTIVE BODY TUBE LOADS DURING FORWARD FLIGHT**  
**HH-16 USA S/N 66-15293**

	DENSITY	GROSS	O.G.	ROTAC	
SYMBOL	ALT.	WEIGHT	STATION	SPEED	CONFIRMATION
0	5000	8615	198.5	324	NOG, SWS
Δ	5000	8610	197.1	324	CLEAR, SWS (DASHED)

**NOTE:**

- 1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY REPORT NO. 209-899-061 INTERPOLATED TO 5000 FEET AND GROSS WEIGHT DERIVED.
- 2- DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT.





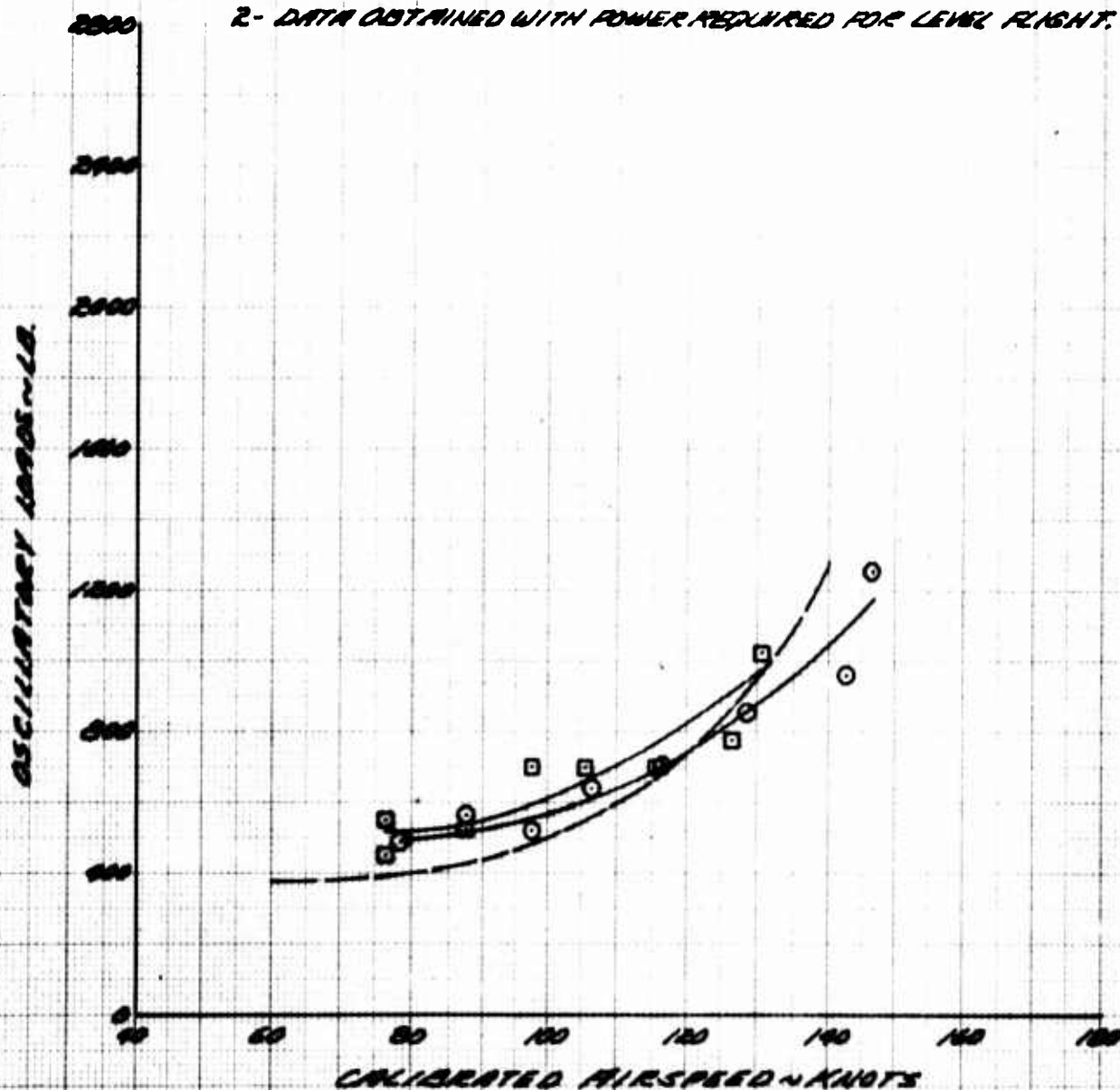
**FIGURE NO. 7**  
**LONGITUDINAL BOOST TUBE LOADS DURING FORWARD FLIGHT**  
**AH-1G USA S/N 66-15293**

	DENSITY	GROSS	C.G.	ROTOR	
	ALTITUDE	WEIGHT	STATION	SPEED	
SYMBOL	N.F.T.	N.L.B.	N.I.N.	N.R.P.M.	CONFIGURATION
○	5000	3270	199.5	324	HOG, STD. NOSE
□	5000	3270	199.5	324	HOG, SNS(CLOSED)

**NOTE:**

1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY  
 REPORT NO. 209-099-091 INTERPOLATED TO 5000 FEET  
 AND 3270 POUNDS.

2- DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT.

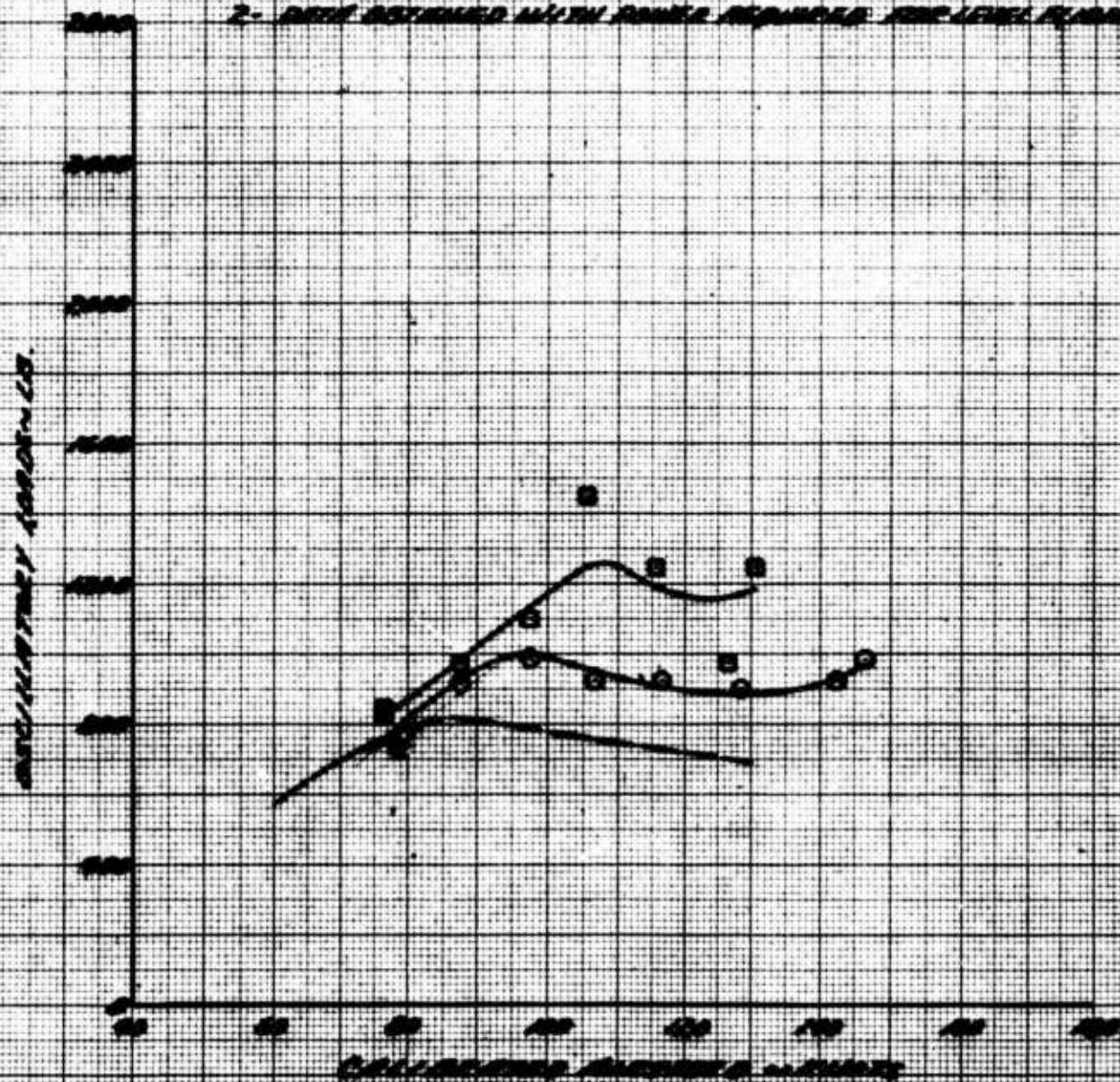


**Figure 1A-8**  
**Low Altitude Performance Data**  
**Altitude 1000 to 1500 Feet**

	Altitude	Weight	Wt.	Wt.	Configuration
	Altitude	Weight	Wt.	Wt.	Configuration
0	1000	3270	194.5	326	100, 570, 1000
0	1000	3270	194.5	326	100, 570, 1000

**NOTE:**

- 1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY REPORT LR 222-233-001 INTERPOLATED TO 500 FEET AND 1000 FEET.
- 2- DASHED CURVE WITH POWER REQUIRED FOR LEVEL FLIGHT.





**FIGURE No. 9**  
**COLLECTIVE BOOST TUBE LOADS DURING FORWARD FLIGHT**  
**AH-1G USA S/N 66-15293**

	DENSITY	GROSS	O.G.	ROTOR	
	ALTITUDE	WEIGHT	STATION	SPEED	
SYMBOL	~FT.	~LB.	~IN.	~RPM	CONFIGURATION
○	5000	9270	194.5	324	HOB, STD. HOSE
□	5000	9270	194.5	324	HOB, SHS (CLOSED)

**NOTE:**

1- DASHED CURVE DERIVED FROM BELL HELICOPTER COMPANY  
 REPORT NO. 209-039-041 INTERPOLATED TO 5000 FEET  
 AND 9270 POUNDS.

2- DATA OBTAINED WITH POWER REQUIRED FOR LEVEL FLIGHT.

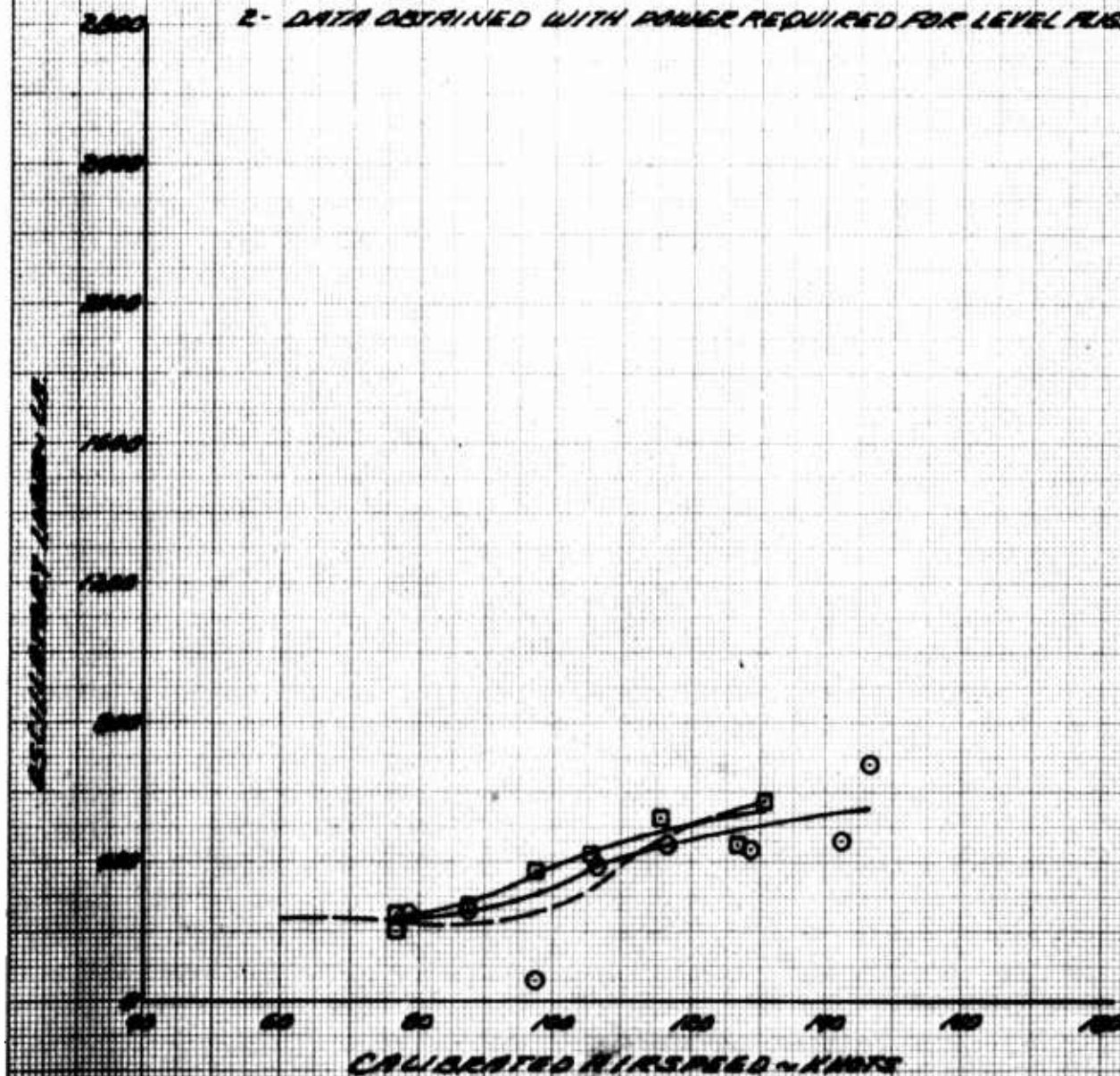
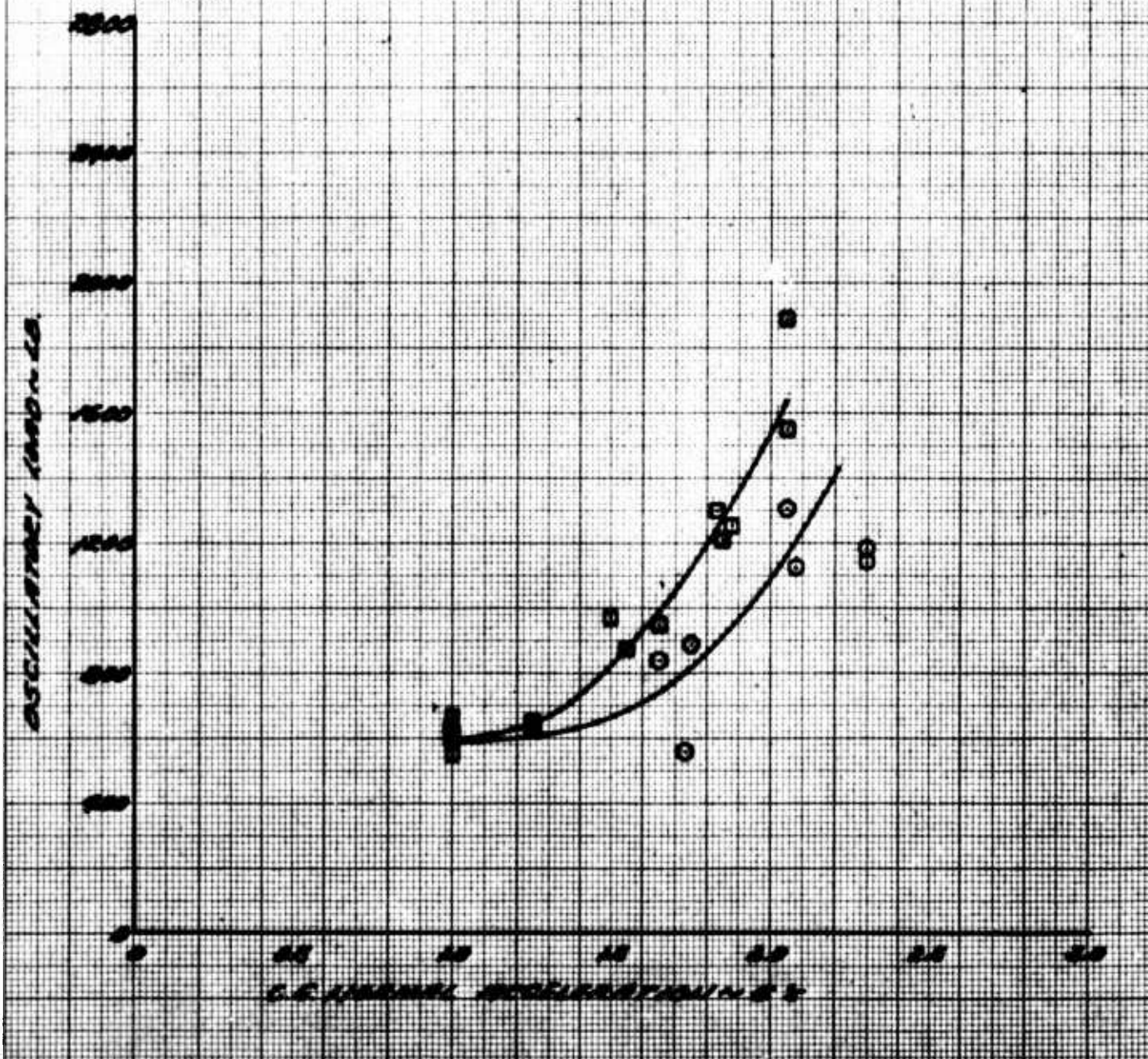


FIGURE 14-10  
Longitudinal Load Factor Limits During Smoothed Pull-Outs  
UH-1C UH-1B 44-15233

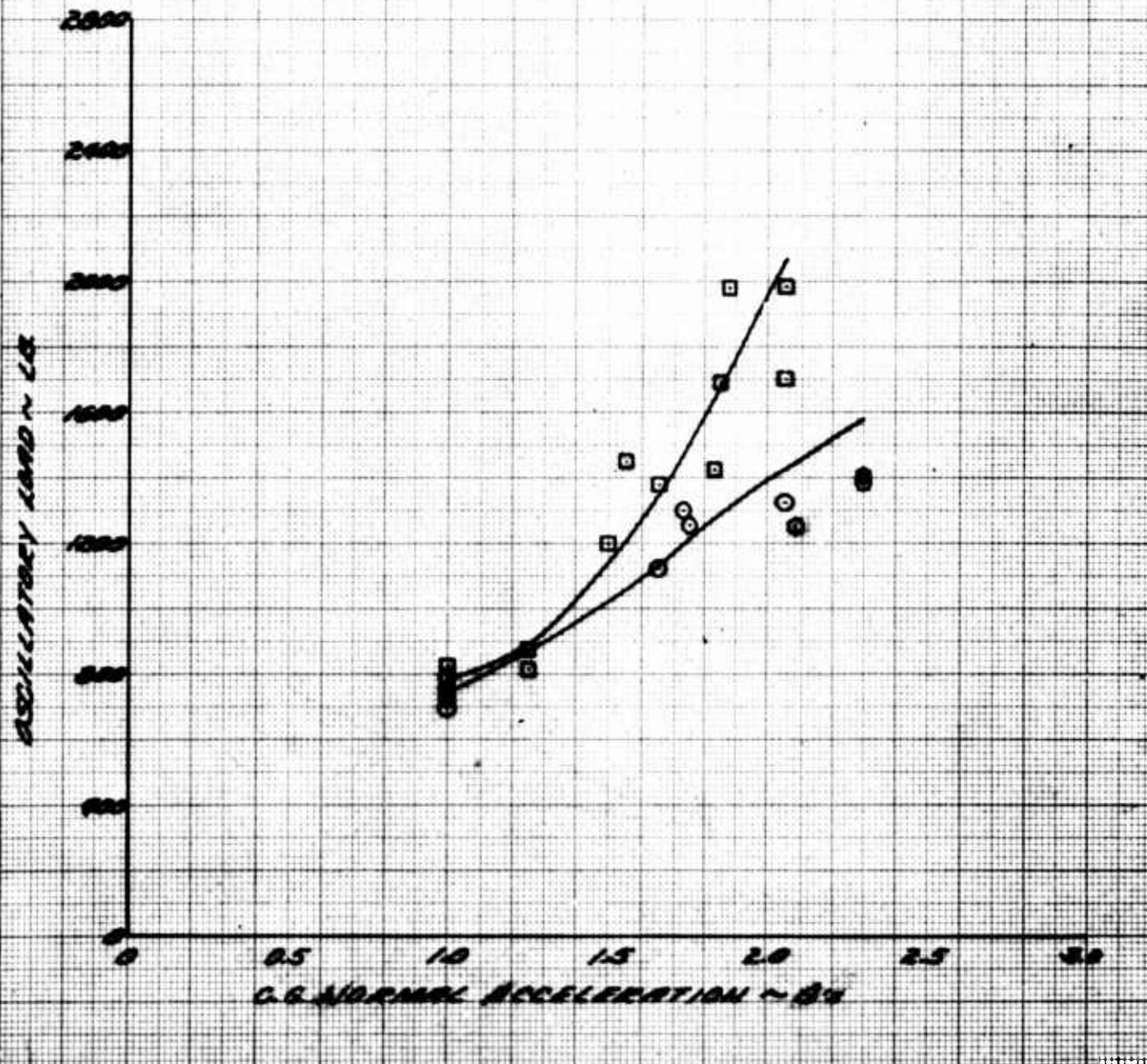
	QUALITY	GRADE	C.G.	WING FROM C.G.		
	HEIGHT	WEIGHT	STATION	SPEED	AIRSPEED	
SYMBOL	FT.	W.B.	INCH	WPM	WTS.	CONFIRMATION
○	5000	7560	195.8	329	14.5	CLEAR, STD. WGT
□	5000	7560	195.8	329	14.5	CLEAR, STD. WGT
○	OBTAINED FROM BELL HELICOPTER COMPANY REPORT NO. 209-099-041 AT 1500 FT., 8200 LB., C.G. STATION 199 IN. AND AIRSPEED DURING PULL-OUT OF 12 KNOTS C.R.S.					





**FIGURE No. 11**  
**LATERAL BUMP TUBE LOADS DURING SYMMETRICAL PULL-OUT**  
**AH-1B USA SIN 66-15293**

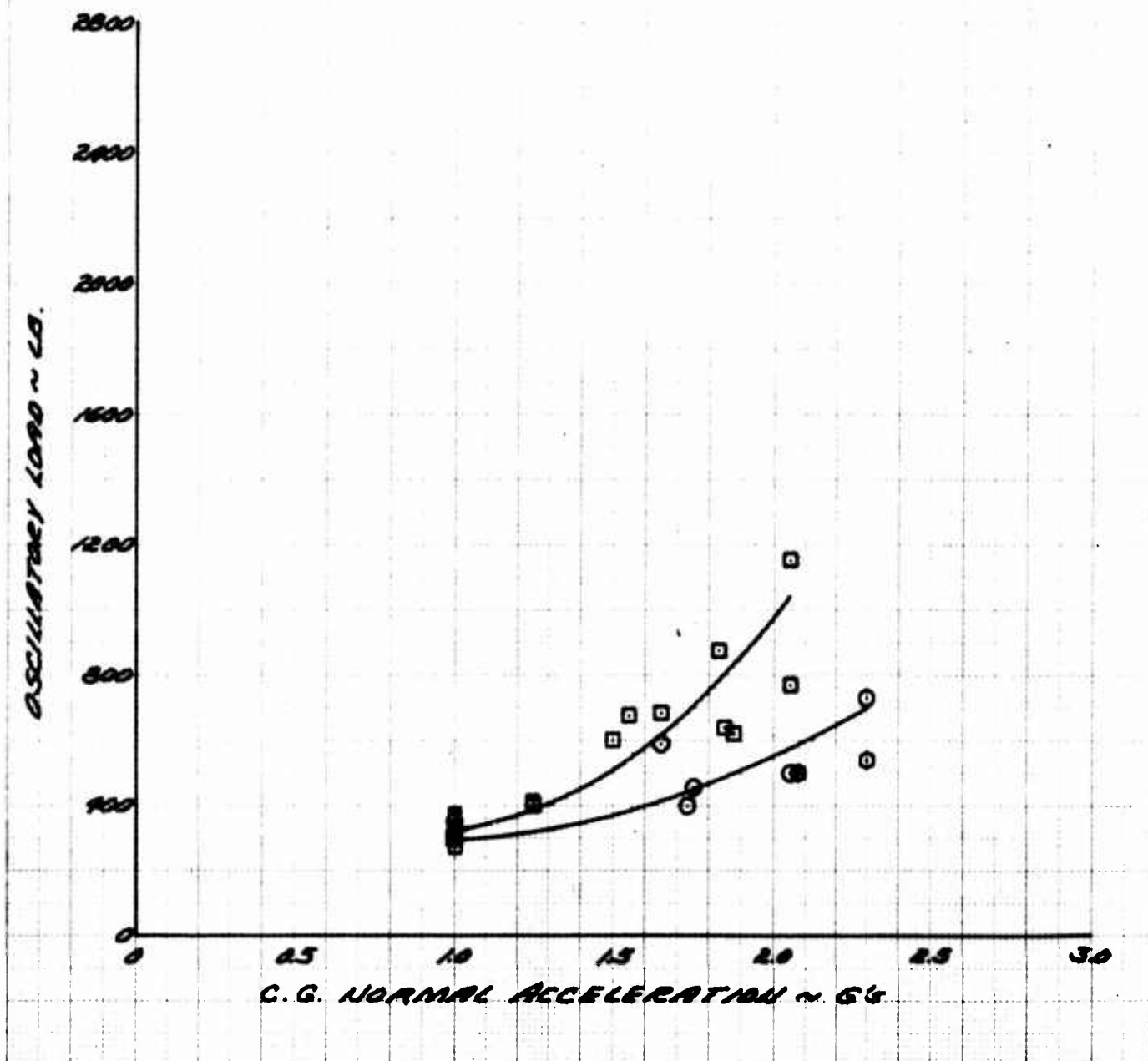
	DENSITY	GROSS	C.G.	ROTOR TRIM CALIB.		
	ALTITUDE	WEIGHT	STATION	SPEED	AIRSPEED	
SYMBOL	FT.	W.LB.	IN.	NRPM	KTS.	COMMENTS
○	3000	7560	195.8	329	116.5	CLEAN, STD. WHEEL
□	3000	7560	195.8	389	116.5	CLEAN, SATURATED
○	OBTAINED FROM BELL HELICOPTER COMPANY REPORT AND 200-099-001 AT 1500 FT., 8200 LB., C.G. STATION 138 IN. AND AIRSPEED DURING PULL-OUT OF 112 KNOTS CASE					



**FIGURE No. 12**  
**COLLECTIVE BOOST TUBE LOADS DURING SYMMETRICAL PULL-OUTS**  
**AH-1G USA SN 66-15293**

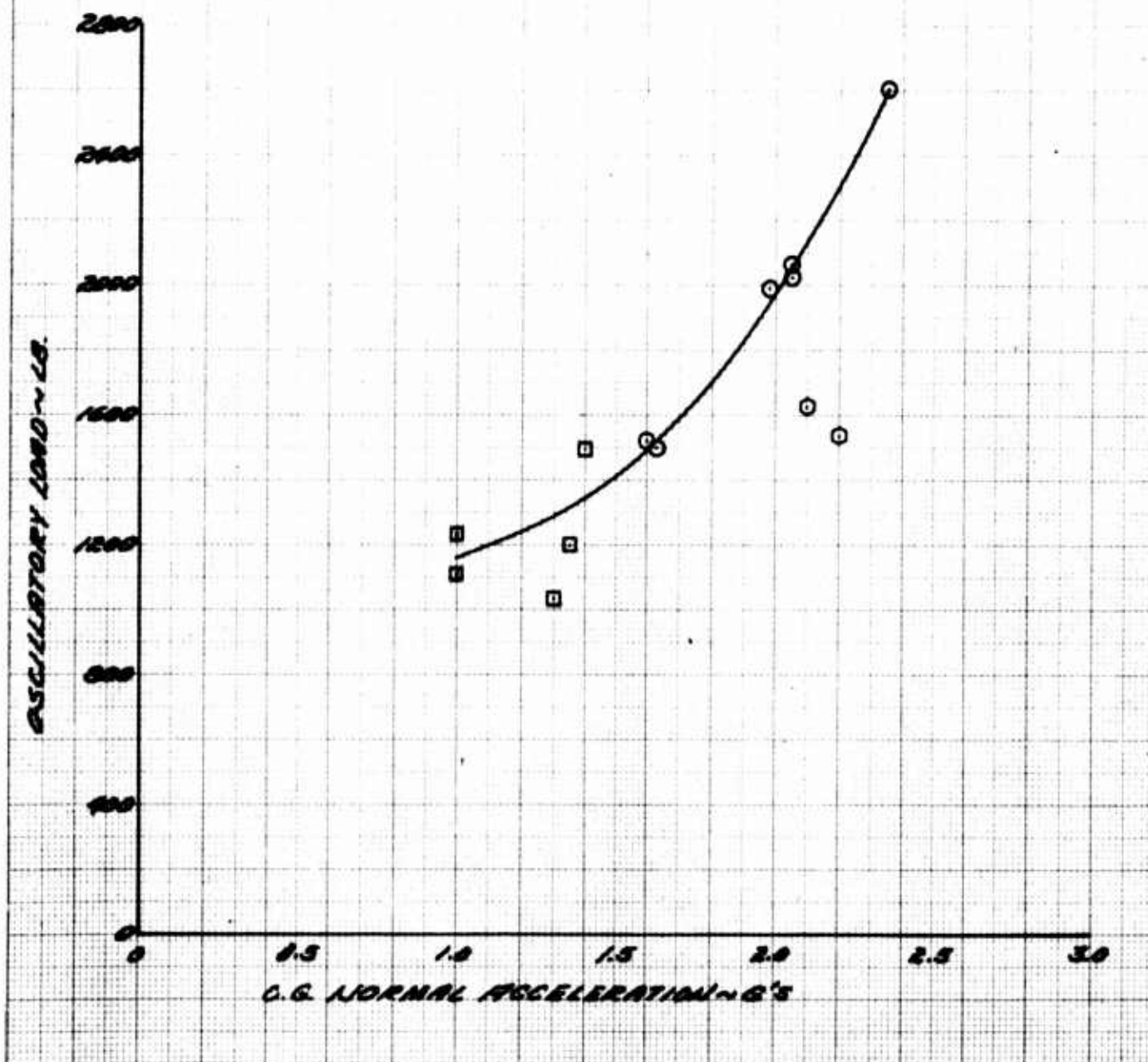
	DENSITY	GROSS	C.G.	ROTAR	TRIM	ORIG.
	ALTITUDE	WEIGHT	STATION	SPEED	AIRSPED	CONFIGURATION
SYMBOL	~FT.	~LB.	~IN.	~RPM	~KTS.	
○	5000	7560	195.8	320	116.5	CLEAN, STD. NOSE
□	5000	7560	195.8	320	116.5	CLEAN, SNS(CLOSED)

○ OBTAINED FROM BELL HELICOPTER COMPANY REPORT NO. 209-099-001 AT 1500 FT., 8200 LB., C.G. STATION 199 IN. AND AIRSPEED DURING PULL-OUT OF 112 KNOTS CAS.



**FIGURE No 13**  
**LONGITUDINAL BOOST TUBE LOADS DURING SYMMETRICAL PULL-OUTS**  
**AH-1G USA SN 66-15293**

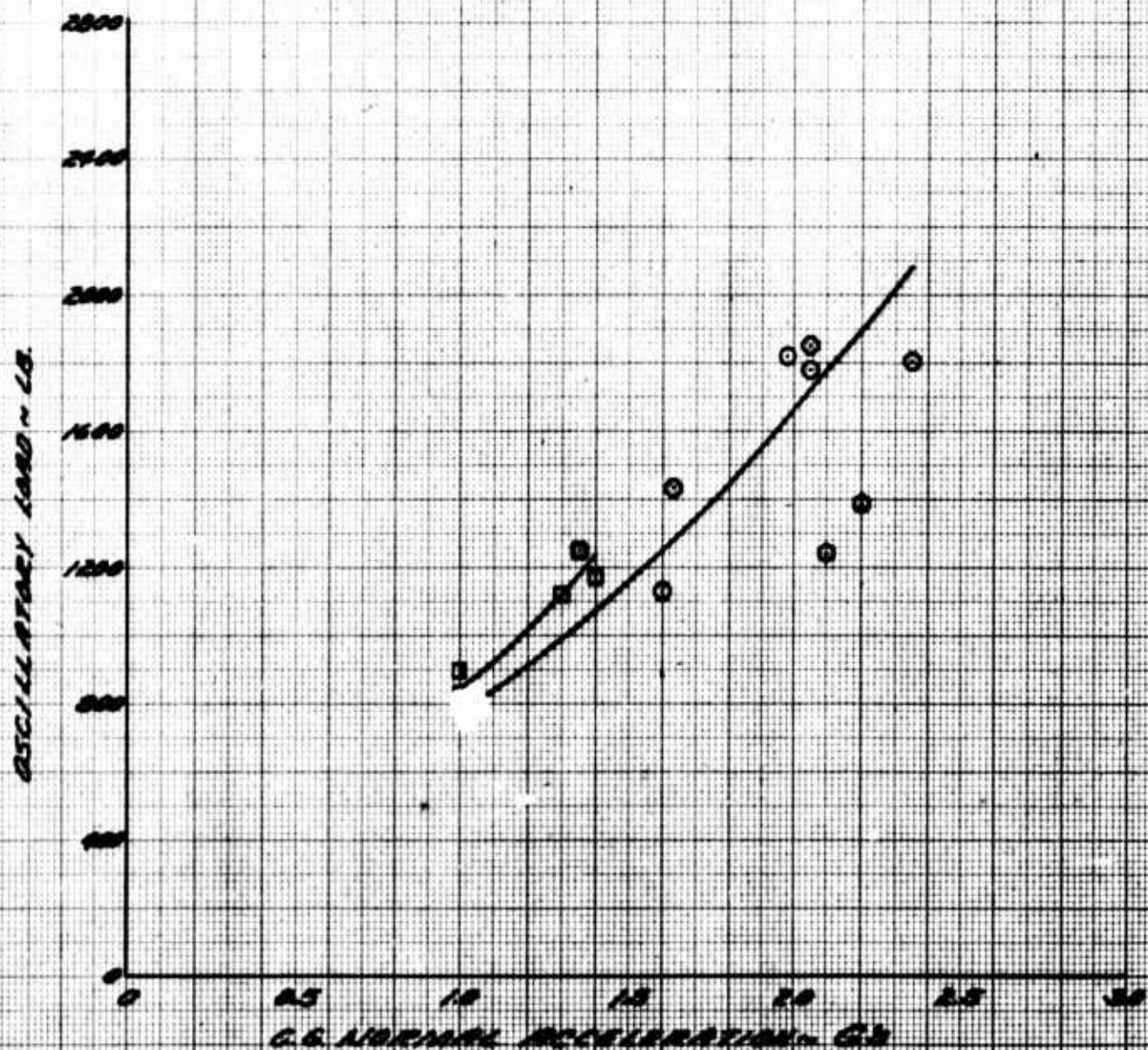
	DENSITY	GROSS	C.G.	ROTOR	TRAIN	CAUS.
	ALTITUDE	WEIGHT	STATION	SPEED	AIRSPEED	CONFIGURATION
SYMBOL	~ FT.	~ LB.	~ IN.	~ RPM	~ KTS.	
○	5000	7560	195.8	324	141.5	CLEAN, STD. NOSE
□	5000	7560	195.8	324	141.5	CLEAN, SAS(CLOSED)
○	OBTAINED FROM BELL HELICOPTER COMPANY REPORT NO. 209-099-041 AT 1500 FT., 8200 LB., C.G. STATION 194 IN. AND AIRSPEED DURING PULL-OUT OF 149.5 KNOTS GAS.					





**FIGURE 141F**  
**LATERAL BRIST TUBE LOADS DURING SYMMETRICAL PULL-OUT**  
**AH-1G USA JAN 66-15293**

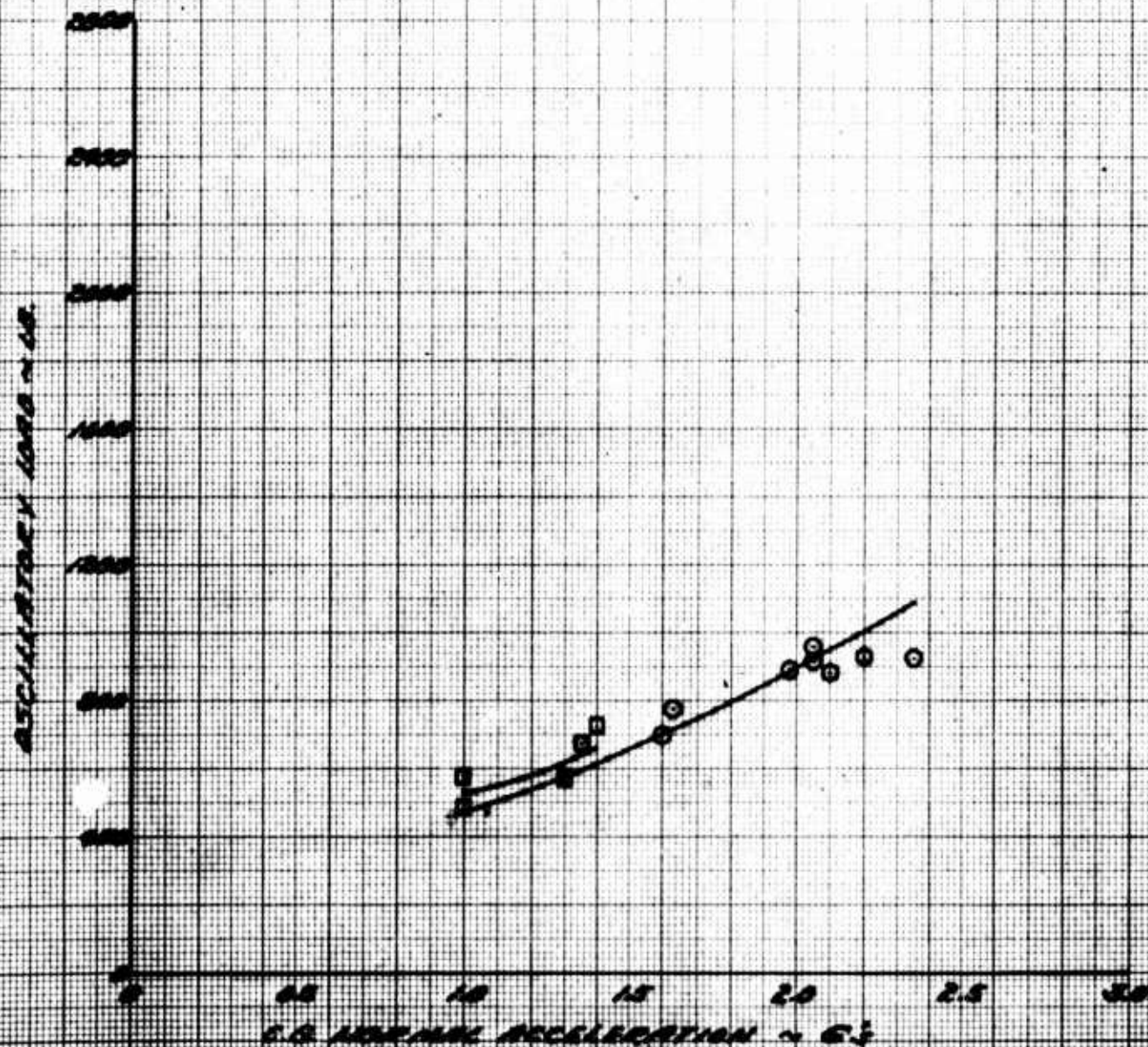
	DENSITY	GRADE	O.G.	ROTOR	TEAM	CLAR
	ALTITUDE	WEIGHT	STATION	SPEED	AIRSPED	
SYMBOL	WFE	WLB	WHL	WHR	WTR	CONFIGURATION
○	5000	7500	196.8	329	191.5	CLEAN, STD. HOSE
□	5000	7500	196.8	329	191.5	CLEAN, SWS(CLOSED)
○	OBTAINED FROM BELL HELICOPTER COMPANY REPORT NO. 209-099-001 AT 1500 FT, 8200 LB, O.G. STATION 196.8 IN AND AIRSPEED DURING PULL-OUT OF 199.5 KNOTS CTS.					



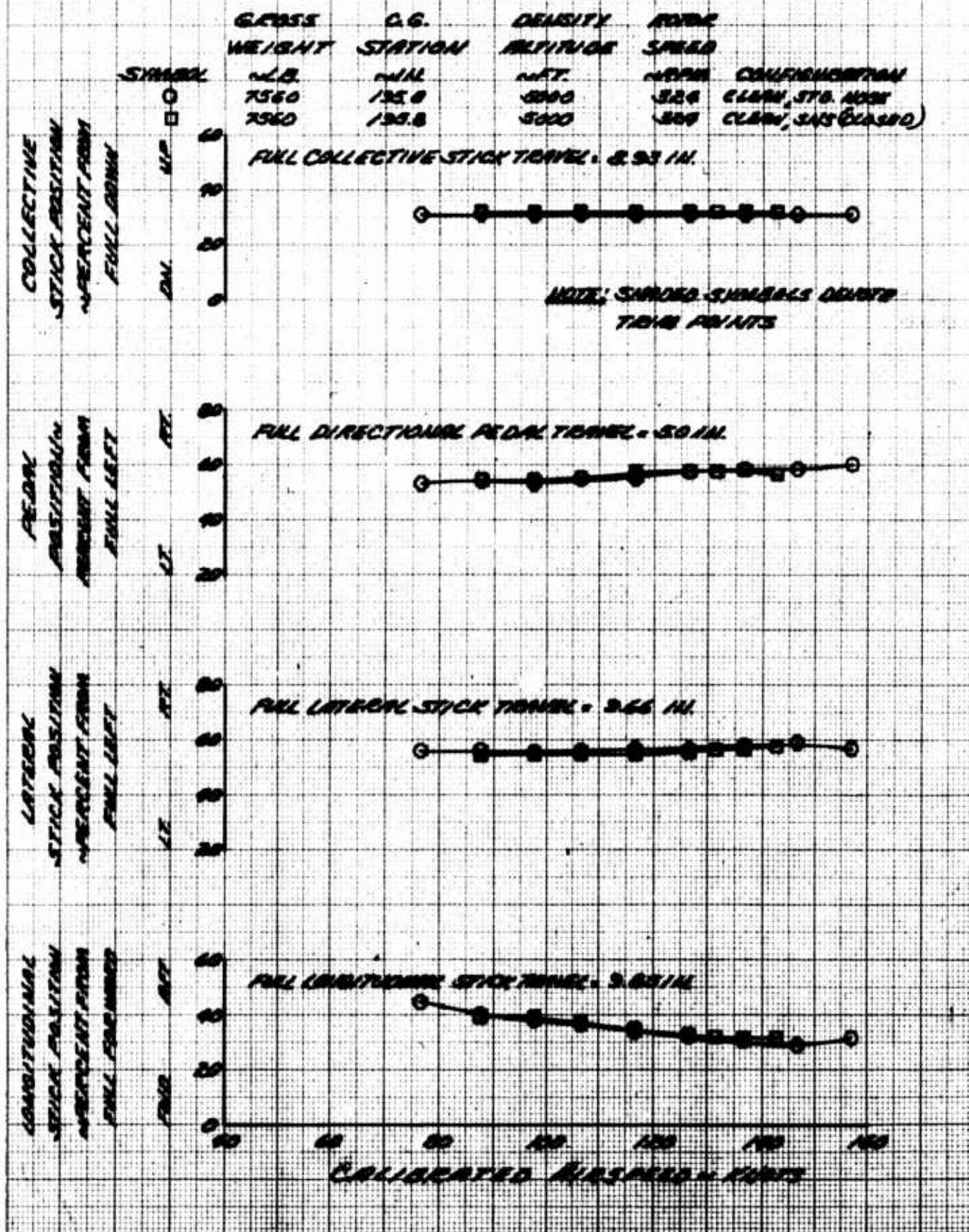


**FIGURE No. 15**  
**COLLECTIVE BOOST TUBE LOADS DURING SYMMETRICAL PULL-OUTS**  
**RH-16 USR SIN 66-15293**

	DENSITY	GROSS	C.G.	ROTOR TRIM CALIB.		
	ALTITUDE	WEIGHT	STATION	SPEED	AIRSPEED	
SYMBOL	NET	NLB	NIN	NRPM	NKTS	CONFIGURATION
○	5000	7560	195.8	329	141.5	CLIMB, STD. LASE
□	5000	7560	195.8	329	141.5	CLIMB, SWS (CLOSED)
○	OBTAINED FROM BELL HELICOPTER COMPANY REPORT NO. 209-039-001 AT 1500 FT., 8000 LB., C.G. STATION 190 IN. AND AIRSPEED DURING PULL-OUT OF 149.5 KNOTS CAS.					

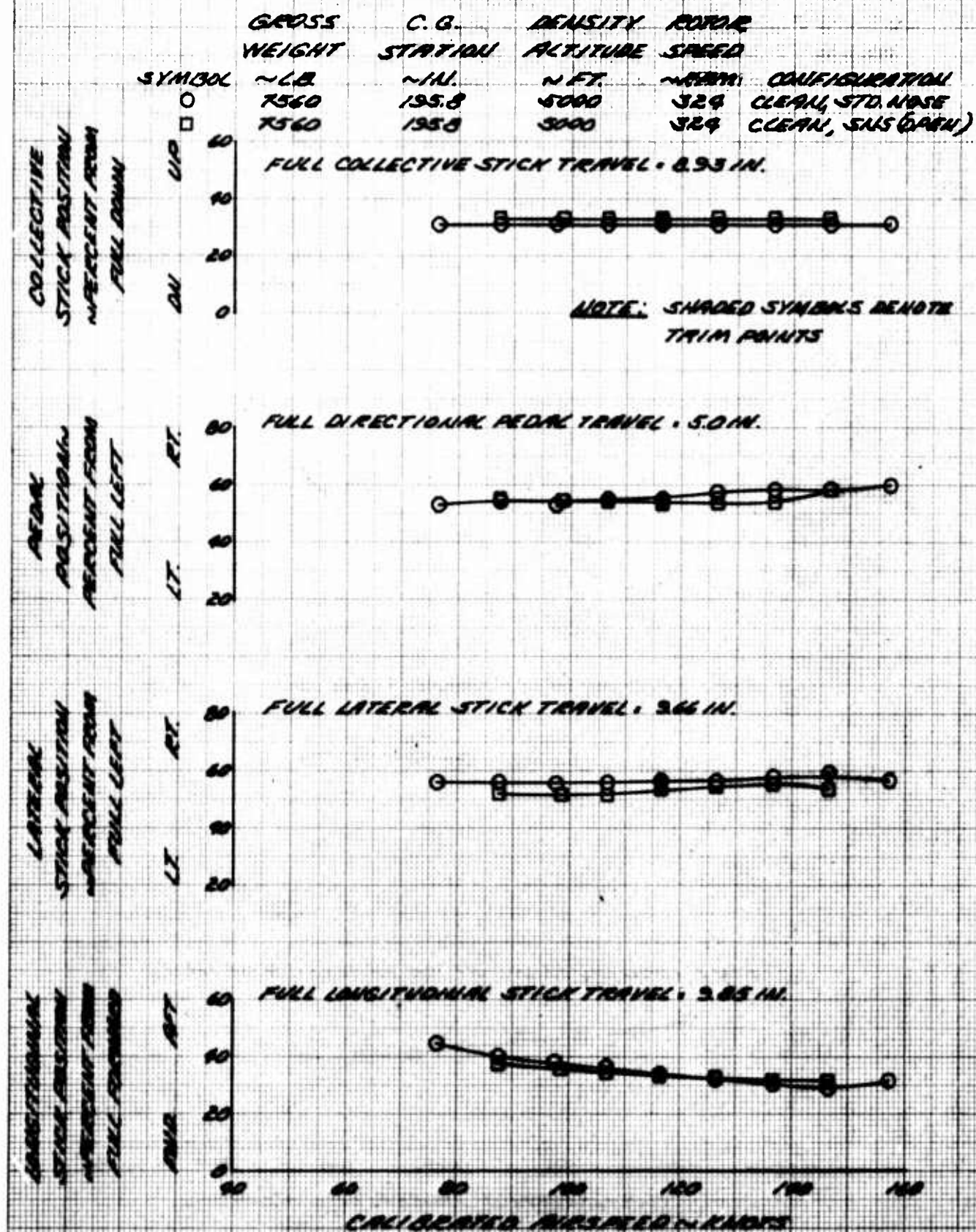


**FIGURE No. 16**  
**STATIC LONGITUDINAL STABILITY**  
**LEVEL FLIGHT**  
**RH-1G USA SN 66-15293**

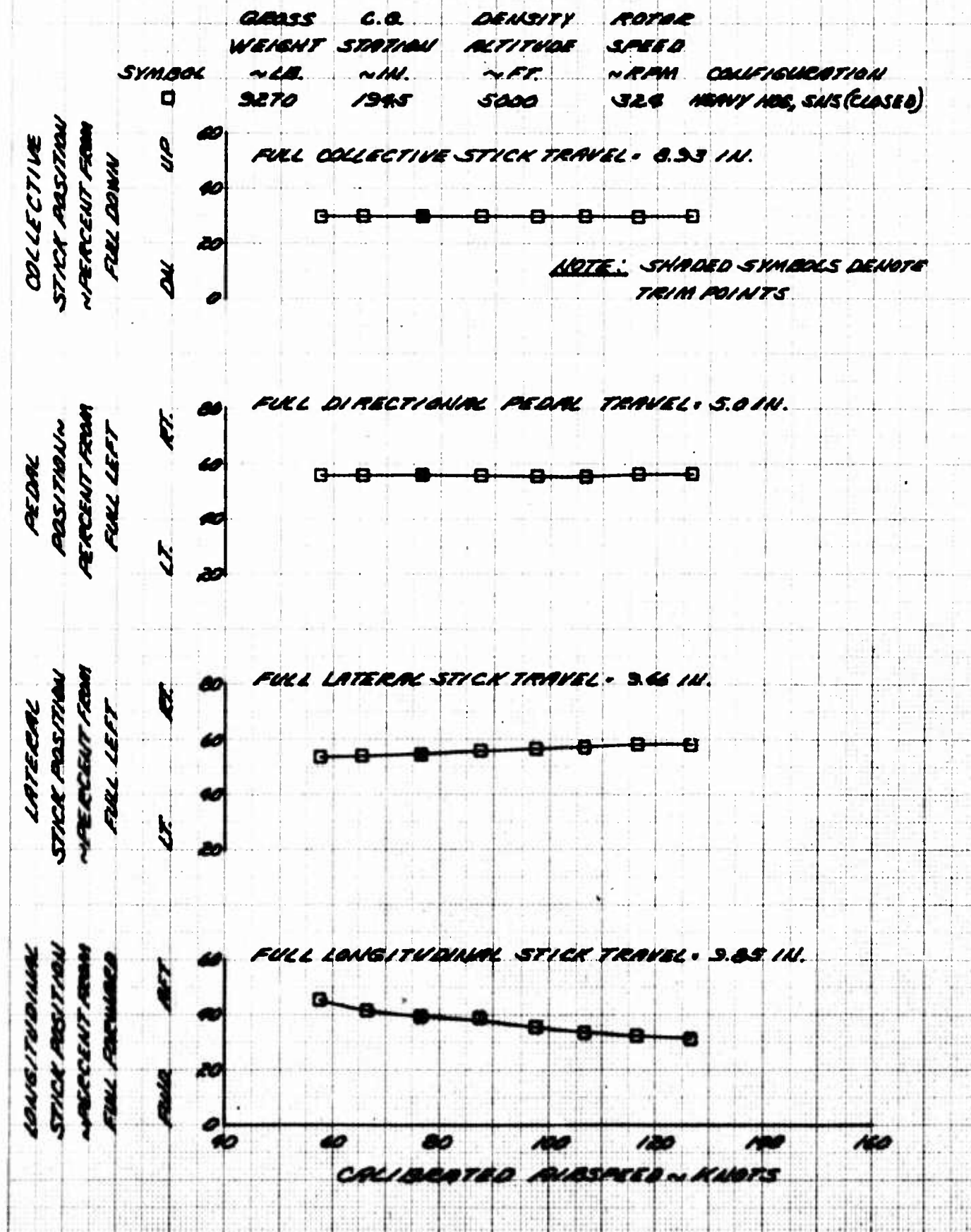




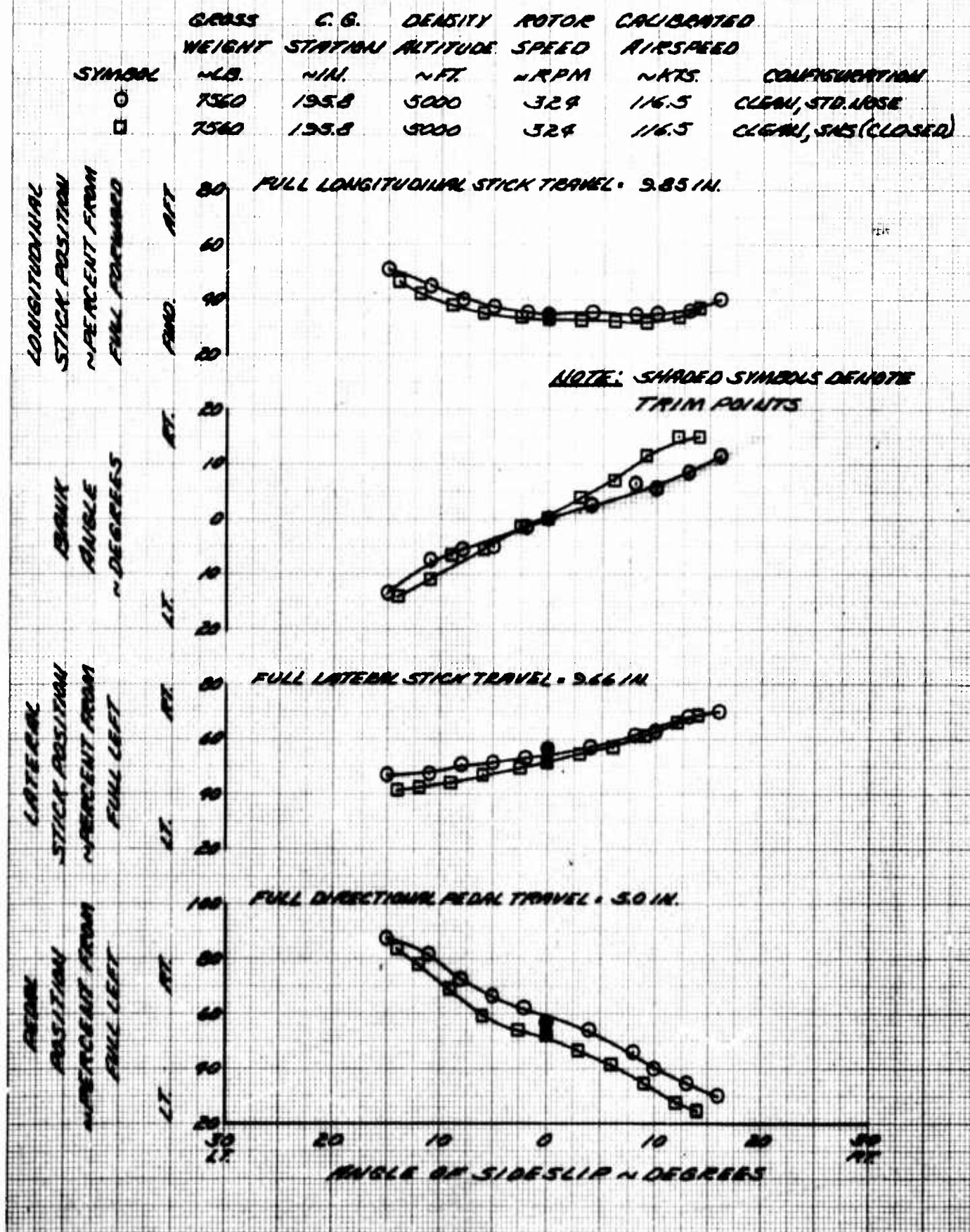
**FIGURE NO. 17**  
**STATIC LONGITUDINAL STABILITY**  
**LEVEL FLIGHT**  
**AH-1G USA S/N 66-15293**



**FIGURE No. 18**  
**STATIC LONGITUDINAL STABILITY**  
**LEVEL FLIGHT**  
**AH-1G USA SN 66-15293**



**FIGURE No. 19**  
**STATIC LATERAL - DIRECTIONAL STABILITY**  
**LEVEL FLIGHT**  
**AH-1G USA S/N 66-15293**





**FIGURE No 20**  
**STATIC LATERAL-DIRECTIONAL STABILITY**  
**LEVEL FLIGHT**  
**AHIG USA SN 46-15293**

	<b>GROSS</b>	<b>C.G.</b>	<b>DENSITY</b>	<b>ROTOR CALIBRATED</b>	
	<b>WEIGHT</b>	<b>STATION</b>	<b>ALTITUDE</b>	<b>SPEED</b>	<b>AIRSPEED</b>
<b>SYMBOL</b>	<b>WLB</b>	<b>WIM</b>	<b>WFT</b>	<b>WPM</b>	<b>WTS</b>
□	9270	194.8	5000	329	76.5
					<b>CONFIGURATION</b>
					HEAVY HNG, SAS(CLOSED)

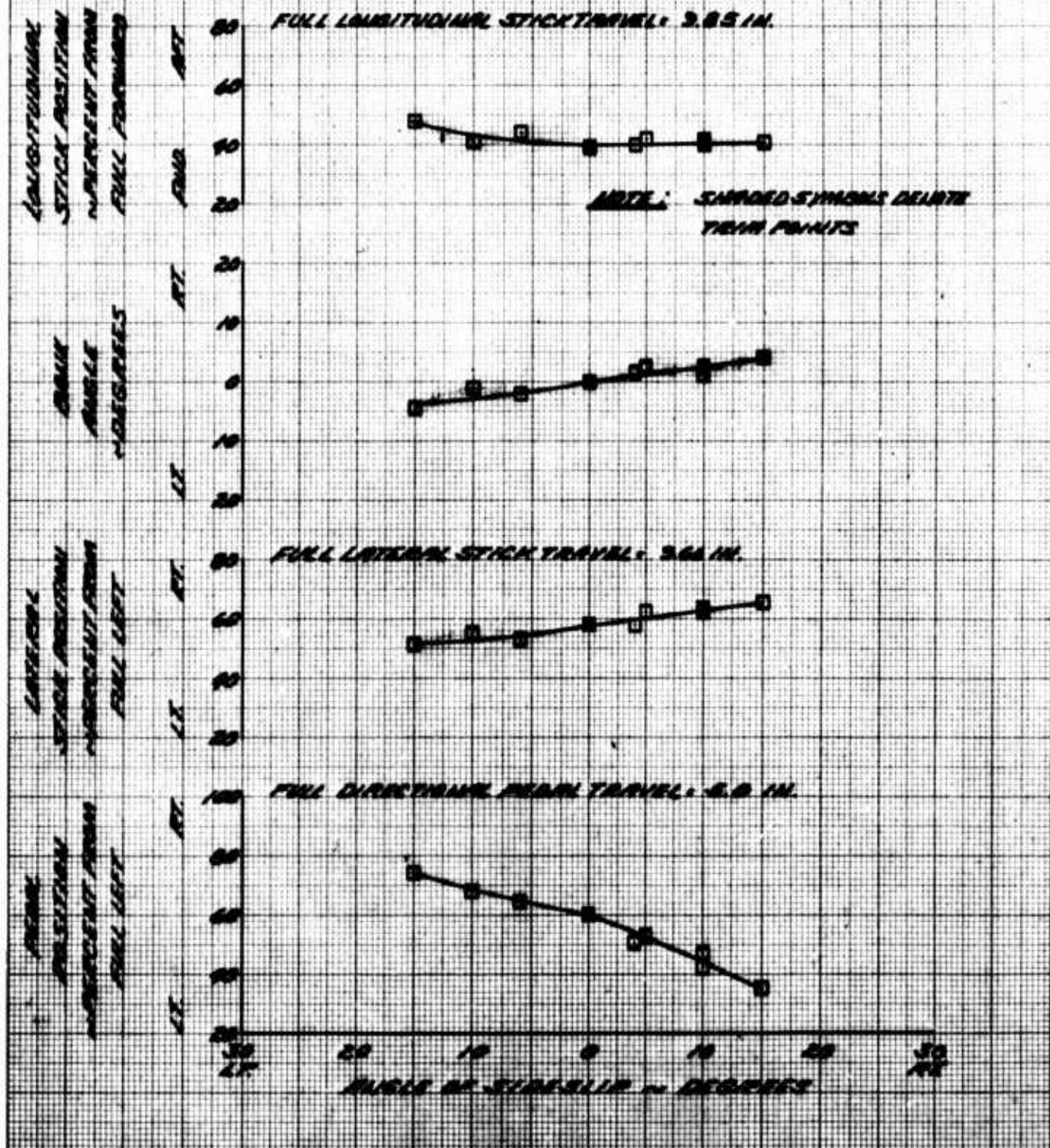


FIGURE No. 21  
VIBRATION CHARACTERISTICS  
AH-1G USA S/N 66-15293  
CO-PILOT VERTICAL

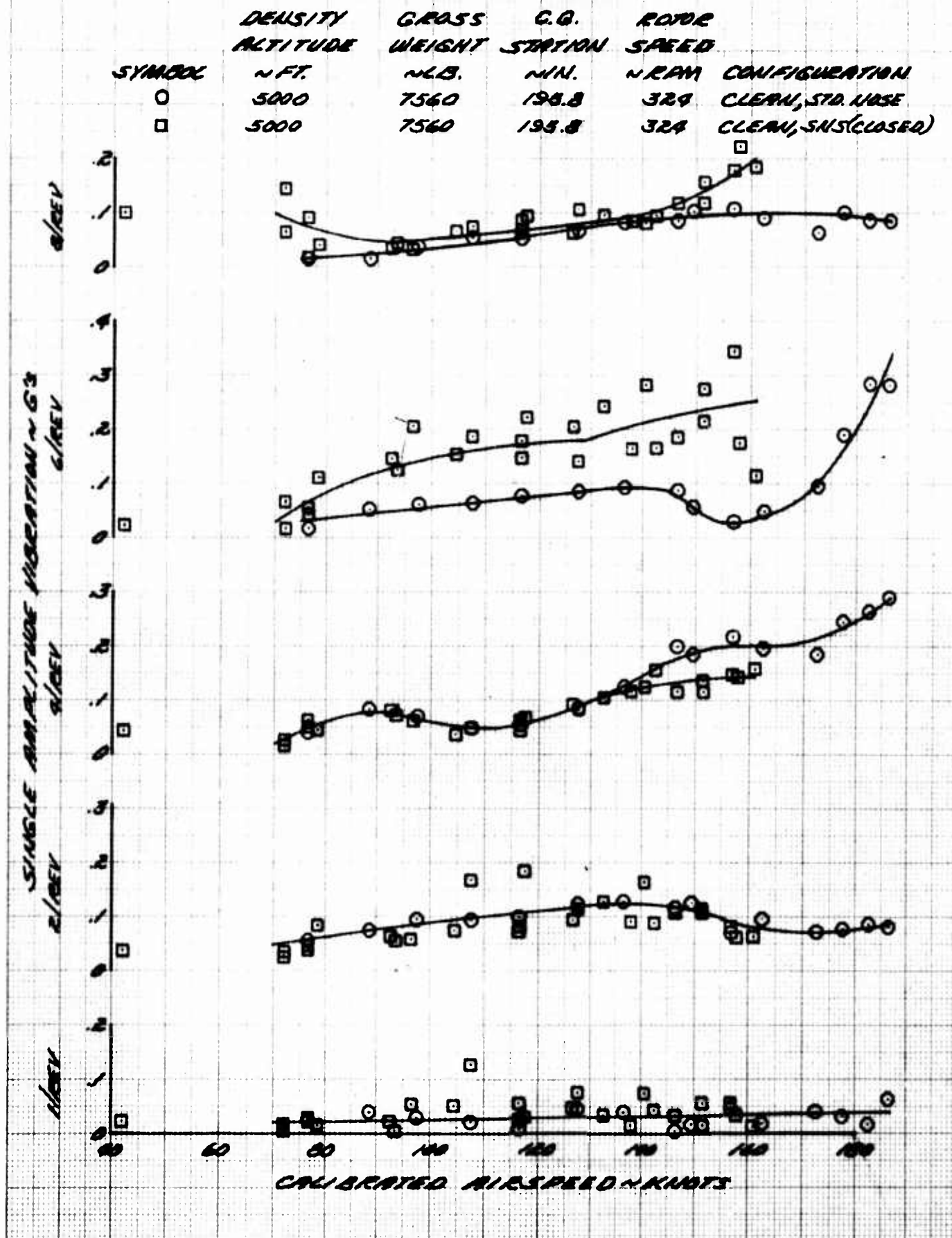


FIGURE No. 22  
VIBRATION CHARACTERISTICS  
AH-1G USA SIN 66-15293  
CO-PILOT LATERAL

SYMBOL	DENSITY ALTITUDE ~FT.	GROSS WEIGHT ~LB.	O.G. STATION ~IN.	ROTOR SPEED ~RPM	CONFIGURATION
○	5000	7560	198.8	324	CLEAN, STD. NOSE
□	5000	7560	198.8	324	CLEAN, SUS (CLOSED)

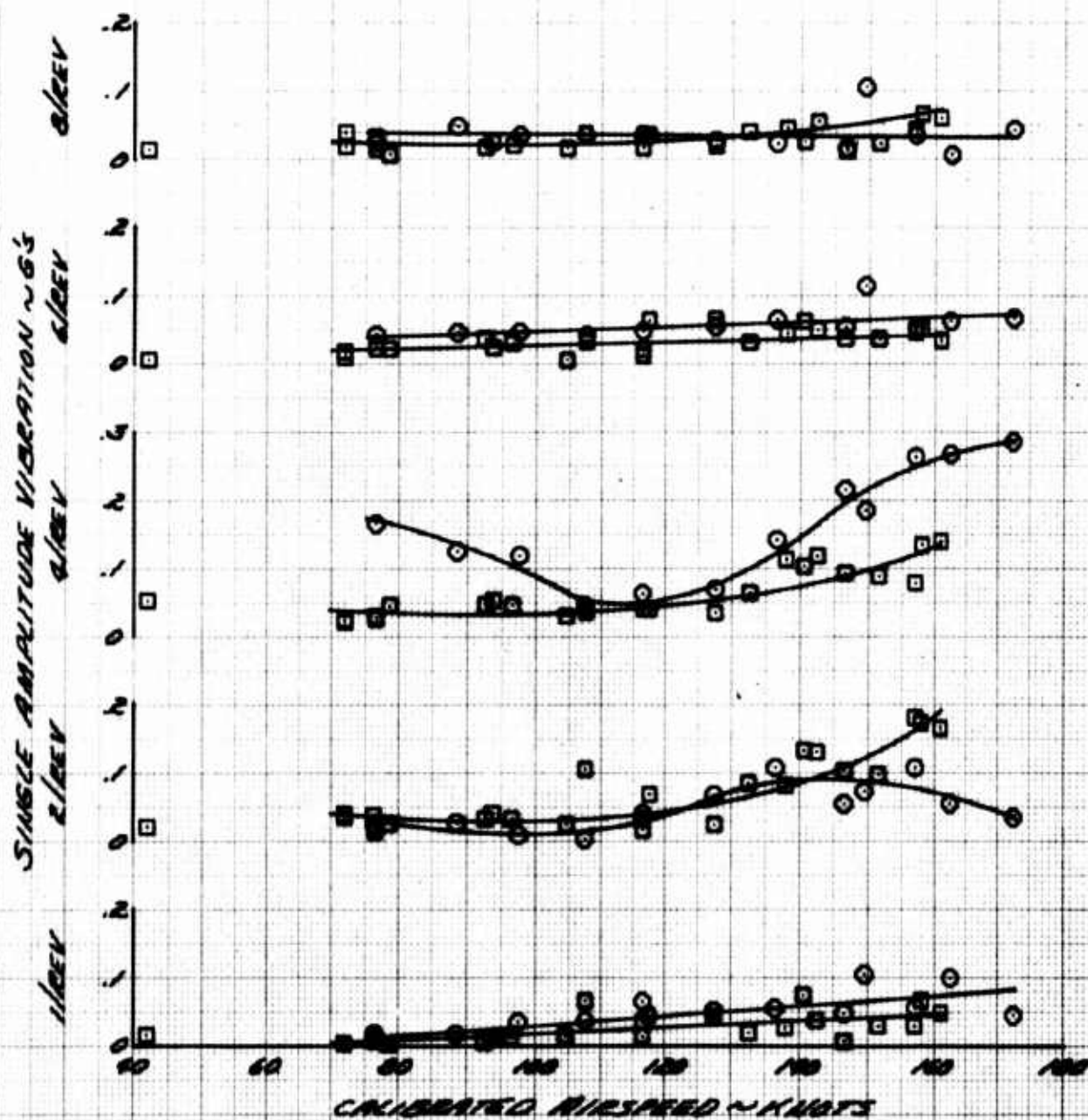




FIGURE No. 23  
VIBRATION CHARACTERISTICS  
AH-1G USAF 66-15293  
CO-PILOT VERTICAL

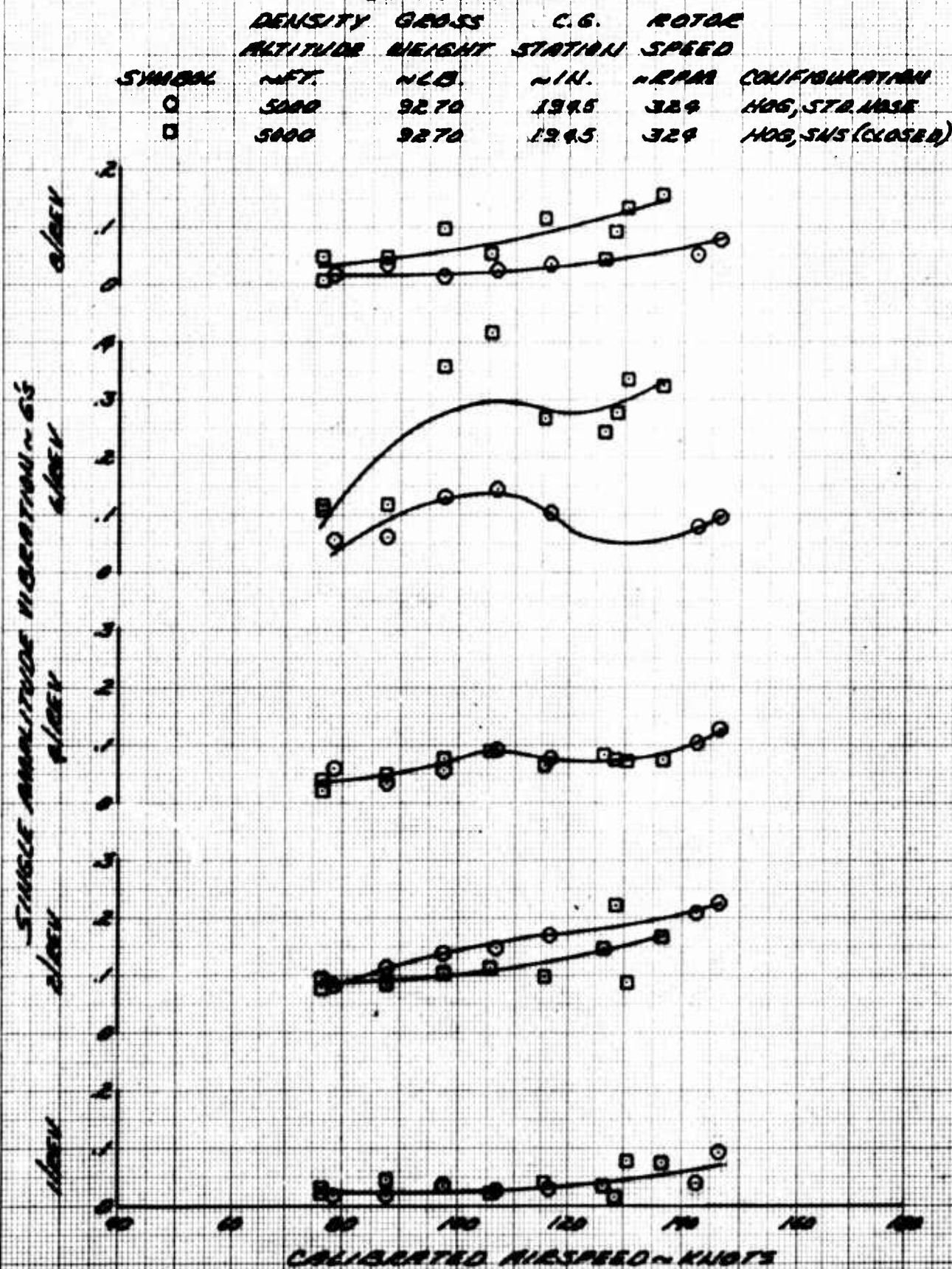
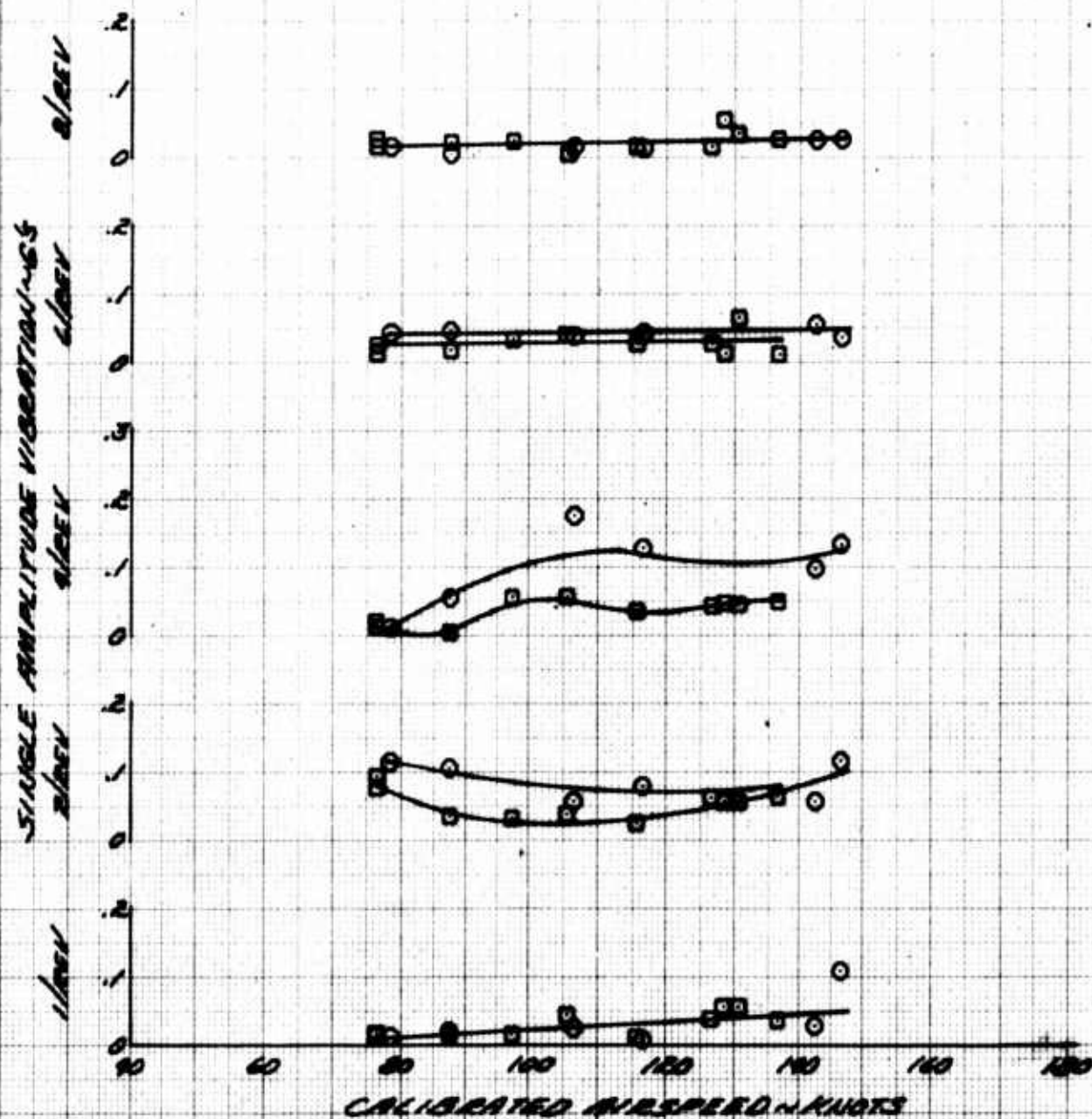


FIGURE NO. 29  
VIBRATION CHARACTERISTICS  
AH-1G USA SN 66-15293  
CO-PILOT LATERAL

SYMBOL	DENSITY ALTITUDE ~FT.	GROSS WEIGHT ~LB.	C.G. STATION ~IN.	ENGINE SPEED ~RPM	CONFIGURATION
○	5000	9870	199.5	329	HOG, STD. NOSE
□	5000	9870	199.5	329	HOG, SNS (CLOSED)



## APPENDIX III. TEST INSTRUMENTATION

1. A swivel-mounted pitot-static airspeed head was installed on a boom which extended approximately 5 feet in front of the nose of the helicopter. This airspeed head was used as a source for the sensitive altitude and airspeed systems. Vanes attached to the boom were used to measure angles of attack and sideslip. Sensitive instrumentation was installed to measure the following parameters:

a. Pilot's Panel

Longitudinal cyclic stick position  
Lateral cyclic stick position  
Collective stick position  
Pedal position  
Boom airspeed  
Boom altitude  
Rotor rpm  
Angle of attack  
Angle of sideslip  
Gas producer speed ( $N_1$ )  
Engine rpm ( $N_2$ )  
Exhaust gas temperature  
Normal acceleration (G)  
Rate of climb

b. Engineer's Panel

Hi-torque pressure  
Lo-torque pressure  
Rotor rpm  
Standard airspeed  
Standard altitude  
Gas producer speed ( $N_1$ )  
Outside air temperature  
Exhaust gas temperature  
Fuel used  
Oscillograph record number

c. Oscillograph

Longitudinal stick position  
SCAS longitudinal position  
Pitch angle  
Pitch rate  
Lateral stick position  
SCAS lateral position

Roll angle  
Roll rate  
Pedal position  
SCAS pedal position  
Yaw angle  
Yaw rate  
Angle of sideslip  
Angle of attack  
Collective position  
Throttle position  
Normal acceleration (G)  
Linear rotor rpm  
Rotor blip  
Voltage monitor  
Pilot's event  
Engineer's event  
Tail rotor torque  
Tail rotor blade angle  
Horizontal stabilizer position  
Lateral and vertical vibration at copilot's station  
FS 79, water line (WL) 52, butt line (BL) 10 right

d. Oscillograph Strain Gage

Control link/tube, BHC P/N 209-030-124-1  
Control link/tube, BHC P/N 209-030-124-3  
Control link/tube, BHC P/N 209-030-124-5  
Tail boom longeron, BHC P/N 209-030-806-15  
SNS structure (gage D8, Itek package)  
SNS structure (gage B5, Itek package)  
SNS structure (gage E8, Itek package)  
SNS structure (gage B4, Itek package)  
Horizontal stabilizer chordwise bending  
Horizontal stabilizer beamwise bending  
Horizontal stabilizer torsional bending



## APPENDIX IV. STANDARD AH-IG OPERATING LIMITATIONS AND DIMENSIONS

### LIMIT AIRSPEED ( $V_L$ )

Hog or alternate configuration: 180 KIAS below a 3000-foot  $H_D$ ; decrease 8 KIAS per 1000 feet above 3000 feet

All other configurations: 190 KIAS below a 4000-foot  $H_D$ ; decrease 8 KIAS per 1000 feet above 4000 feet

### GROSS WEIGHT - CENTER OF GRAVITY ENVELOPE

Forward limit: Below 7000 pounds, FS 190; linear decrease from FS 190 at 7000 pounds to FS 192.1 at 9500 pounds

Aft limit: Below 8270 pounds, FS 201; linear decrease from FS 201 at 8270 pounds to FS 200 at 9500 pounds

### SIDESLIP LIMITS

Five degrees at 190 KIAS; linear increase to 20 degrees at 60 KIAS

### RPM LIMITS

#### Rotor:

294 to 324 rpm, continuous operation  
339 rpm, maximum for autorotation

#### Engine:

6000 to 6400 rpm, 0 to 70 knots  
6400 to 6600 rpm, continuous operation  
6600 rpm, maximum  
6750 rpm, maximum at or below 91-percent gas producer speed ( $N_1$ )

### TEMPERATURE AND PRESSURE LIMITS

Engine oil temperature	93°C
Transmission oil temperature	110°C
Engine oil pressure	25 to 100 psi
Transmission oil pressure	30 to 70 psi
Fuel pressure	5 to 20 psi

#### T53-L-13 ENGINE LIMITS (Installed)

Normal rated (maximum continuous)	625°C
Military rated (30-minute limit)	645°C
Starting and acceleration (5-second limit)	675°C
Maximum for starting and acceleration	760°C
Torque pressure	50 psi

#### PHYSICAL CHARACTERISTICS

Aircraft length (rotors turning)	635.7 inches
Fuselage length	535.1 inches
Maximum fuselage width (including stub wings)	124.0 inches
Maximum fuselage width (without stub wings)	36.0 inches

#### MAIN ROTOR

Rotor diameter	528 inches
Chord	27 inches
Disc area	1520.4 ft <sup>2</sup>
Blade area (each)	49.5 ft <sup>2</sup>
Solidity ratio	0.0651

#### AIRCRAFT WEIGHTS

Empty weight (S/N 66-15355)	5789 pounds
Design gross weight	6600 pounds
Maximum gross weight	9500 pounds

UNCLASSIFIED

Security Classification

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13. ABSTRACT  The Phase I airworthiness and flight characteristics tests of the AH-1G helicopter with the mock-up stabilized night sight (SNS) installed indicated a feasibility for further development utilizing the actual SNS equipment. No significant changes in the handling qualities due to the SNS modification were noted during the tests. The static, proof load test results indicate that the structure is adequate to withstand the required loads. The flight test data from the three nonrotating control boost tubes show higher loads for the AH-1G in both the SNS and standard nose configurations than the Bell Helicopter Company test data. The control boost tube loads reached the maximum permitted at conditions short of the published envelope. Testing was terminated early to obtain instrumented components (rotor blade, drag brace and pitch link) so the flight envelope and/or fatigue life of these components could be more accurately determined. These tests are scheduled to be completed during Phase II with the actual SNS installed. The vertical six-per-revolution vibrations at the copilot's seat exceed military specification requirements in the SNS configuration.		

DD FORM 1473  
1 NOV 66REPLACES DD FORM 1473, 1 JAN 64, WHICH IS  
OBSOLETE FOR ARMY USE.

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14.	KEY WORDS	LINK A		LINK B		LINK C	
		ROLE	WT	ROLE	WT	ROLE	WT
	Phase I Airworthiness and flight characteristics AH-1G helicopter Mock-up SNS Feasibility Handling characteristics Static, proof load test results Structure is adequate Boost tube loads Instrumented components Phase II Vibrations						

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